

Thermal Energy Storage with **Transcritical Recuperative Two-Phase Cycles**

Motivation Cycle efficiency as the key aspect

Transcritical Rankine cycle are discussed for Pumped Thermal Energy Storage (PTES) systems with the ambient or a latent storage as low-temperature heat reservoir and a sensible storage as high temperature reservoir [1]. But transcritical Rankine cycles have significant disadvantages:

— Exergy losses due to mismatch of the heat capacity flows of subcooled liquid (3 \rightarrow 4) and superheated vapor (6 \rightarrow 1) in the recuperator

— Exergy losses in heat pump cycles due to the isenthalpic throttling process (4 \rightarrow 5), which can only be overcome by using a two-phase expander

Due to the importance of the cycle efficiency for the round trip efficiency advanced [2], measures for the improvement of the cycle are required.



Application PTES with sensible Storage



15 °C Water at ambient conditions **15 °C**

Results

Method

Thermodynamic concept of a transcritical cycle

A novel transcritical cycle [3] is used to increase the heat pump (HP) and power cycle (PC) efficiency. It is based on a former subcritical version of the Recuperative Two-Phase Cycle (RTPC) [4]. The key aspects is the introduction of an asymmetric mixture composed out of a main fluid (e.g. isobutane) with a high fraction (around 95 mole%) and an auxiliary fluid (e.g. dodecane), which leads to a phase change instead of a pure superheating of the working fluid on the low-pressure side of the recuperator (6 \rightarrow 1). Thereby the capacity flows in the recuperator are equalized and the exergy losses decrease. Furthermore, this leads in a heat pump cycle to lower throttling losses and in a power cycle to lower preheating losses.

Transcritical Recuperative Two-phase Cycle in Heat Pump mode



As a consequence, these cycles are more efficient than transcritical Rankine

Fluid selection and cycle design

different With asymmetric two hydrocarbon mixtures for each cycle second law efficiencies of over 70 % can be reached, thus the round trip efficiency is 51,9 %. However, these must be taken as preliminary results, due to high variability of the non-linear optimization problem and due to the uncertainty of the thermodynamic properties of the asymmetric mixtures.

Assumptions	
<i>P_{el}</i> compressor HP	100 kW
ΔT_{min} of HXs	5 K
η_{is} of all machines	0,8
Pressure drop	0 Pa
Heat losses	0 kW
Electrical losses	0 kW



cycles with hydrocarbons and even more with CO₂ as the working fluid. Furthermore, the maximum pressure in the cycle is slightly lower.

Figures:

Fig. 1: Example of a conventional transcritical Rankine heat pump cycle with the working fluid isobutane for a low temperature level of 15 °C and a high temperature level between 150 °C and 300 °C.

Fig. 2: Example of the novel transcritical Recuperative Two-phase Cycle in heat pump mode (HP-RTPC-TC) with the working fluid mixture composed out of 95 mole% isobuane and 5 mole% dodecane for a low temperature level of 15 °C and a high temperature level between 150 °C and 300 °C. The shown isobars are 1 bar, 5 bars and 10 bars up to 100 bars.

Fig. 3: Concept of a Pumped Thermal Energy Storage (PTES) system based on two transcritical Recuperative Two-phase *Cycles, one in heat pump mode and one in power cycle mode and a thermocline storage system filed with molten salt.*

Fig. 4: T, *H* diagram for the entire PTES system: heat pump and power cycle connected by the temperature profile of a storage. As an approximation the siloxane D6 is used for the calculation of the profile.

Literature:

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