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# Textile Reinforcement Structures for Concrete Construction Applications – A Review

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## Keywords:

- A. Textile-Reinforced Concrete (TRC)
- B. Textile Reinforcement Structure
- C. Robot-Supported Manufacturing
- D. Non-Crimp Fabric

## Abstract:

The use of non-metallic, textile reinforcement structures in place of steel reinforcement is a key component in making concrete constructions more sustainable and durable than they currently are. The reason for this is the corrosion resistance of textile reinforcements, which makes it possible to reduce the thickness of the concrete cover and at the same time extend the service life of concrete structures. This reduces the amount of cement required and thus also the emission of the greenhouse gas carbon dioxide (CO<sub>2</sub>). By means of textile manufacturing technologies, customized, load-adapted reinforcement topologies can be adjusted to the requirements of highly stressed and well-designed concrete components. The objective of this paper is to give an overview of recent research literature dedicated to textile reinforcement structures that are already used for concrete applications in the construction industry as well as those currently under development. Therefore, textile reinforcement structures, which are divided into one-, two- and three-dimensional topologies, as well as common materials used for textile-reinforced concrete (TRC) are reviewed. Most research has so far been devoted to two-dimensional textile reinforcement structures. Furthermore, novel approaches to the fabrication of textile reinforcement structures for concrete applications based on robotic yarn deposition technologies are addressed.

## 1. Introduction

The construction and operation of buildings in the European Union (EU) is responsible for roughly half of the use of extracted materials and energy as well as a third of the water consumption in the EU.<sup>1</sup> In addition, the sector causes approximately a third of the greenhouse gas emissions in the European Union.<sup>2,3</sup> The main driver for the emission of greenhouse gases in the construction sector is the production of cement, which alone accounts for about 8 % of global greenhouse gas emissions.<sup>4</sup> Reducing resource usage and emissions of greenhouse gases in the construction sector are therefore central challenges facing academia, governments and the industry alike.

One possible solution to reduce the use of concrete, and therefore of cement, involves the substitution of conventional steel reinforcement with a reinforcement made of non-metallic technical textiles.<sup>5</sup> While reinforcing steel requires a comparatively thick concrete cover to prevent/delay corrosion, technical textiles do not corrode in contact with air and thus do not deteriorate in mechanical strength and stiffness, allowing the concrete cover to be reduced to a minimum.<sup>6</sup> This leads to considerable savings of concrete and therefore reductions in resource usage and greenhouse gas emissions<sup>7-10</sup>. For example, a pedestrian and cyclist bridge built in Albstadt-Ebingen (Germany) in 2015 using carbon-fiber-based reinforcement decreased the required amount of concrete by 60 % and resulting carbon dioxide (CO<sub>2</sub>) emissions by 26 % compared to a steel-reinforced alternative.<sup>9</sup> Although on a mass base, carbon fiber reinforcements as the main representatives of technical textiles in the construction industry are more energy-intensive in its production than steel reinforcements and hence also more carbon emissions intensive, the fact that far less of it is needed to reinforce concrete allows for total emissions savings. Direct comparison of the production-related emissions of 1 kg of steel reinforcement (2.3 kg CO<sub>2</sub> equivalents) with one kilogram of carbon fiber reinforcement (19.7 kg CO<sub>2</sub> equivalents) shows that carbon dioxide emissions are around 8.6 times higher.<sup>10</sup> However, for a conventional building product like a double wall, Scope et al. found that up to 22 times less carbon fiber reinforcement is required by weight instead of steel reinforcement.<sup>8</sup> In their life cycle sustainability assessment, they compare two steel-reinforced concrete variants of a double wall to two carbon fiber-reinforced concrete variants. Similarly to the reinforcement, the concrete for the carbon fiber-reinforced variants is also more energy-intensive to produce due to the high cement content, although up to 32.5 % concrete is saved compared to the steel-reinforced variants.<sup>8</sup> For the total double wall, embodied carbon emissions can be reduced by up to 25 % when using carbon fiber-reinforced concrete instead of steel-reinforced concrete.<sup>8</sup>

Although there are several extensive summaries addressing the technology of textile-reinforced concrete (e.g.,<sup>11-13</sup>), there is a lack of summarising research literature focused on the textile reinforcement structures used in concrete and their current developments. Therefore, the aim of this paper is to summarize the state of the art of textiles used as concrete reinforcement as well as ongoing research in this area. This paper is focused on textile reinforcement structures utilizing continuous fibers. The topic of short fibers for concrete reinforcement is only briefly introduced since there have been several comprehensive reviews on this topic recently.<sup>14-17</sup> Also, this review paper is limited to textile reinforcements used within the concrete matrix and therefore does not include textile reinforcements applied to the outside of the concrete, such as lamellae or jackets, as described elsewhere, for example by Tatar and Milev.<sup>18</sup>

The use of technical textiles as reinforcement in concrete has been researched for a long period of time, with first patents being published in the 1980s.<sup>19</sup> In the late 1990s and 2000s, large research efforts in Germany led to the foundation of the new material combination, dubbed textile-reinforced concrete (TRC).<sup>20,21</sup> Other names for this composite material, especially in an international research

context, include textile-reinforced mortar (TRM) and fabric-reinforced cementitious matrices (FRCM).<sup>22</sup>

The basic idea of TRC follows the established principles of steel-reinforced concrete.<sup>5</sup> The concrete matrix has a high compressive strength and can easily be cast into a multitude of shapes while using locally available materials. These advantages have led to concrete becoming the most important construction material and the second most used resource worldwide, just surpassed by water.<sup>23</sup> However, concrete has a comparatively low tensile strength, which can be mitigated using reinforcing materials with high tensile strength, such as steel or technical textiles. Steel-reinforced concrete has been researched and used for nearly two centuries and is one of the cornerstones of the modern construction industry. Steel-reinforced concrete construction is usually realized with various types of reinforcement elements, such as reinforcing steel bars and wires for one-dimensional (1D) reinforcements, welded wire meshes for two-dimensional (2D) reinforcements and reinforcement cages for three-dimensional (3D) reinforcements.<sup>24</sup> A few basic types of steel reinforcement for concrete according to the definition of the German Institute of Standardization e.V. (DIN) in DIN 488 are listed in Table 1.1.

**Table 1.1: Characteristics of steel reinforcement elements following DIN 488<sup>25–28</sup>**

<b>Product form</b>	<b>Yield strength in N/mm<sup>2</sup></b>	<b>Tensile strength in N/mm<sup>2</sup></b>	<b>Elongation at break in %</b>	<b>Nominal diameter in mm</b>	<b>Manufacturing process</b>	<b>Surface condition</b>
<b>Reinforcing steel bar</b>	500	550	2.5	6 – 28	Cold forming	Ribbed
<b>Welded steel wire mesh</b>	500	550	2.5	6 – 28	Cold forming and welding	Ribbed
<b>Reinforcing steel wire</b>	500	550	2.5	4 – 12	Cold forming	Smooth
<b>Reinforcing steel wire</b>	500	550	2.5	4 – 12	Cold forming	Profiled

Currently established textile reinforcements resemble these steel reinforcements in shape, function and application methods, with fiber-reinforced plastic rebars and textile meshes being the most common types of textile reinforcements. The beneficial property of common reinforcement textiles is their resistance to corrosion in contrast to steel reinforcements, which positively affects their long-term strength as well as the required thickness of the concrete cover.

Currently, the two main applications of TRC involve the retrofitting of existing structures<sup>22,29–37</sup> and the production of precast elements,<sup>38–43</sup> as TRC combines low weight and high strength with corrosion resistance. More specific examples of TRC precast elements are facades<sup>44–51</sup> and elements for simple buildings, such as pavillions<sup>52–55</sup> or garages.<sup>39</sup> Another prominent application of TRC is the construction of bridges.<sup>37,56–61</sup> Several bridges of different sizes, ranging from pedestrian to vehicular, have been constructed by means of TRC, some using precast elements, others being cast in situ. In addition, the CUBE in Dresden (Germany) will be the world's first house to be built entirely with TRC.<sup>62–65</sup>

Within this paper, textile reinforcement structures used for concrete reinforcement are classified according to two criteria as shown in Figure 1.1, i.e. their production process and their dimensionality. The production processes are first divided into two categories: conventional textile production processes, using specialised textile machinery, and robotized production methods relying on industrial robots to produce the reinforcement structure. In both categories, various reinforcement textile production methods are used and are therefore discussed in this paper, as shown in Figure 1.1. The second criterion, the dimensionality, is defined by the dimensionality of the

reinforcement effect that is provided by the textile structure. 1D textile structures only offer reinforcement in one direction, while two- and 3D textiles offer reinforcement in two or three directions, respectively.

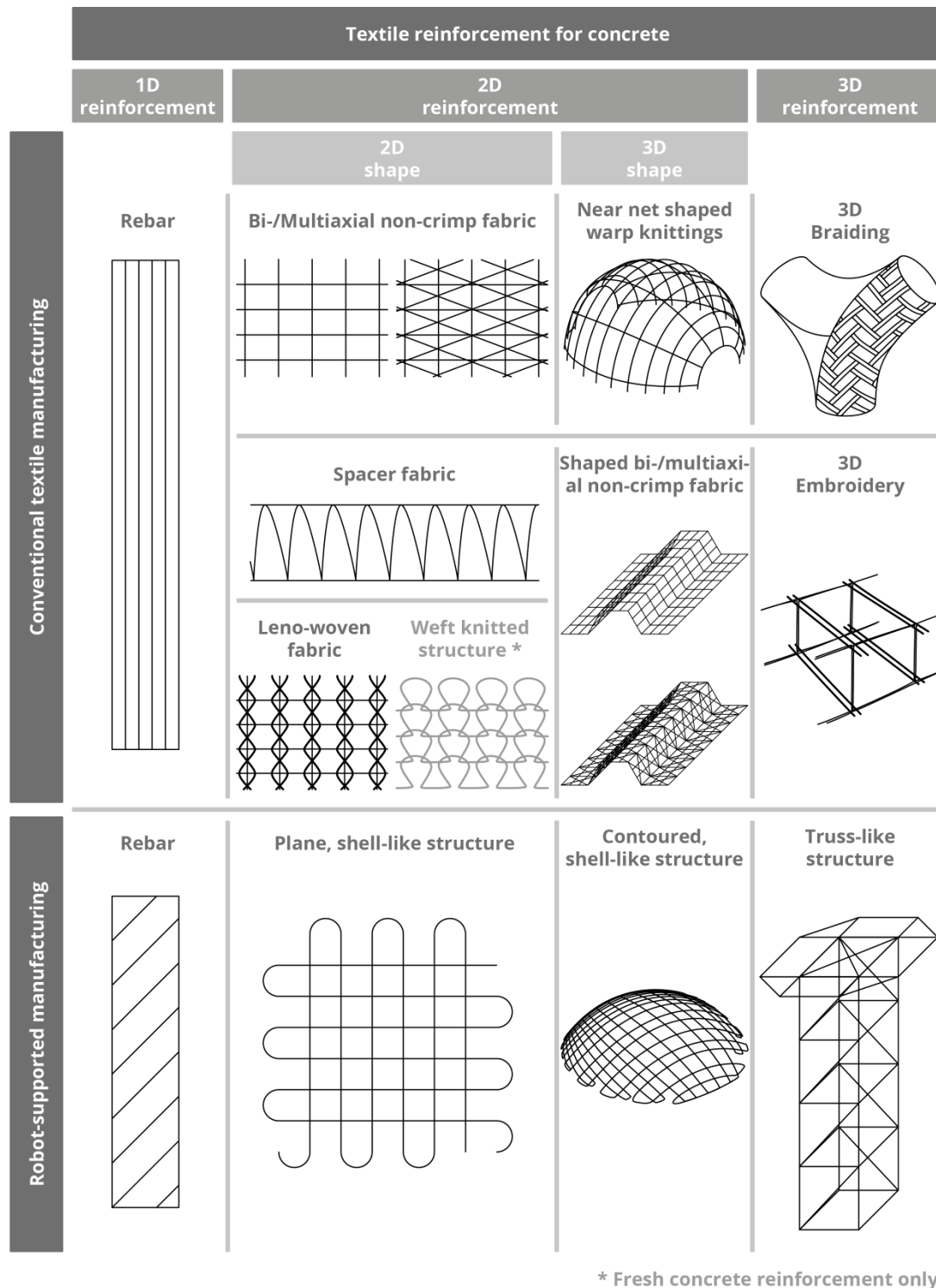


Figure 1.1: Schematic illustrations of different textile reinforcement types for concrete<sup>12,66-74</sup>

After an introduction to the materials used for the production of textile reinforcements for concrete, the structure of this paper follows the system established in Figure 1.1. First, textile reinforcements for concrete produced using specialized textile machinery are discussed, beginning with 1D structures, followed by 2D and 3D structures. Subsequently, textile reinforcements for concrete

produced using industrial robots are discussed. Finally, the findings are summarized and promising new developments for the textile reinforcement of concrete are presented.

## 2. Materials for textile reinforcement structures for construction applications

This chapter provides a summary of common man-made and natural-fiber-based textiles including their functional properties regarding the requirements of reinforced concrete components. Furthermore, this section addresses commonly used impregnation materials for textile reinforcement structures in terms of requirements, such as Young's modulus, inner and outer bond behavior, fire resistance as well as a protective barrier against chemical attacks of alkalis.<sup>75</sup> Impregnation is used synonymously with coating in the cited literature. All mentioned material specifications refer to the application of textile reinforcement in the construction industry. In addition, a short summary of the interfacial transition zone between textile reinforcement and concrete matrix is given, since this area is crucial for the load induction into the reinforcement.

### 2.1. Fiber materials

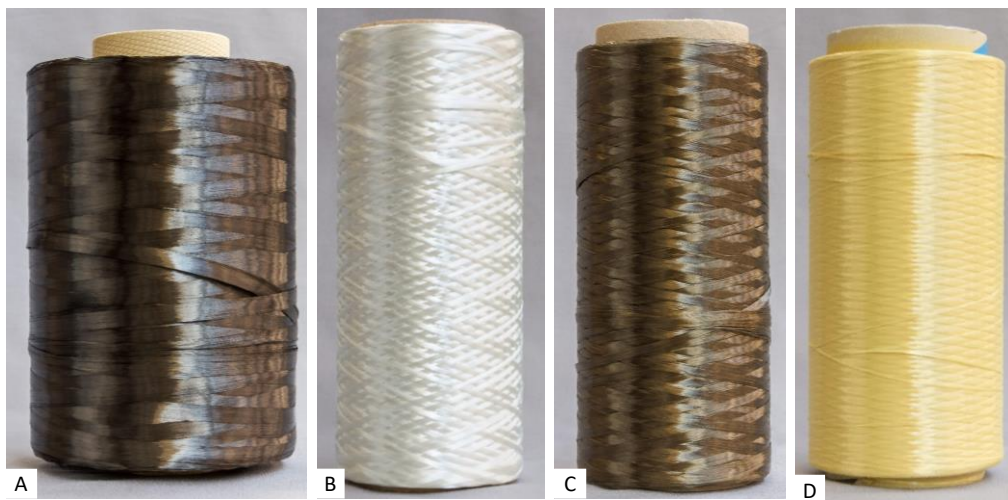
Fibers can be classified into chemical and natural fibers as well as a wide range of raw materials, as there are metal, ceramic and natural fibers in addition to man-made fibers, where synthetic polymer and inorganic fibers are further distinguished.<sup>76</sup> The class of technical fibers with diameters of a few micrometers comprises quasi endless fibers, so-called filaments, bunched together in various forms with up to 144,000 single fibers (144k).<sup>77</sup> Three fundamental reinforcement fiber types for concrete reinforcement are glass fiber (GF), basalt fiber (BF) and carbon fiber (CF) due to their highly anisotropic structure combined with high-strength but anisotropic mechanical properties. Initial efforts to replace steel with man-made fiber-based textile reinforcements started in the 1980s, when standard electric (E-) glass fibers were used to strengthen concrete components instead of reinforcing steel.<sup>69,75</sup> As the alkaline environment of concrete adversely affects the mechanical performance of reinforcement structures based on E-glass fiber, the advanced type of alkali-resistant (AR) glass fiber is superior to E-glass and even better than BF regarding its degradation resistance when exposed to an alkaline environment.<sup>31,76,78-81</sup> Following Bobeth et al.<sup>82</sup>, Wulfhorst<sup>72</sup> and Ehrenstein<sup>83</sup>, Table 2.1.1 gives an overview of the basic properties of selected fiber types for concrete construction applications.

**Table 2.1.1: Properties of selected technical reinforcement materials<sup>69,72,82-85</sup>**

<b>Reinforcement material</b>	<b>Filament diameter in <math>\mu\text{m}</math></b>	<b>Density in <math>\text{g}/\text{cm}^3</math></b>	<b>Tensile strength (roving) in MPa</b>	<b>Breaking strain in %</b>	<b>Young's modulus in GPa</b>
<b>E-glass</b>	9 – 24	2.5 – 2.6	2,400	3.3 – 4.8	72 – 77
<b>AR-glass</b>	9 – 24	2.7	1,800 – 2,000	2.0 – 4.3	21 – 76
<b>Aramid</b>	12	1.5	3,400 – 3,600	2.0 – 4.0	80 – 186
<b>Basalt</b>	9 – 12	2.6	990 – 4,800	1.5 – 3.2	64 – 89
<b>Carbon</b>	5 – 10	1.8	3,000 – 6,000	0.35 – 2.1	240 – 500

Another advantage of AR glass fiber is its lower price per kilogram compared to CF.<sup>86</sup> The alkaline resistance of AR glass fiber is higher compared to that of E-glass fiber but lower than the chemical durability of CF.<sup>69,78</sup> Studies on the reinforcement of concrete structures with aramid fibers (AF) have also been sought through, it should be noted that AF loses considerable strength in alkaline environments.<sup>87-89</sup> Moreover, AF tends to absorb water, which leads to a deterioration of fiber stiffness.<sup>83,82</sup> Nonetheless, progress is driven by research continuously. Basalt fiber with diameters of 9  $\mu\text{m}$  to 12  $\mu\text{m}$  is a technical fiber type used to reinforce concrete components and characterized by

high mechanical and chemical properties comparable with GF.<sup>90-97</sup> GF as well as BF consist of inorganic compounds.<sup>76</sup> Moreover, BF shows very high thermal resistance.<sup>98</sup> Carbon fiber with diameters of 5 to 10  $\mu\text{m}$  is predominantly made of the synthetic polymer polyacrylonitrile (PAN) and offers beneficial properties for strengthening concrete constructions due to its highly anisotropic structure.<sup>69,99-101</sup> Moreover, CF offers the highest resistance to alkaline environments (inert)<sup>69,102</sup> and the highest Young's modulus as well as tensile strength in fiber axial direction in comparison with all mentioned fiber types within the scope of concrete reinforcement.<sup>83</sup> In addition, CF is characterized by the lowest breaking strain compared to other fiber types (Table 2.1.1). Figure 2.1.1 shows a selection of individual ready-to-use fiber materials as semi-finished materials for non-metallic textile reinforcements structures that have already been investigated in previous research projects with the aim of strengthening concrete components in place of steel reinforcements.



**Figure 2.1.1: Selection of already investigated fiber materials for concrete reinforcement structures: A – Carbon fibers, B – Glass fibers, C – Basalt fibers, D – Aramid fibers**

The class of polymer fibers, which is also applied for reinforcing concrete components, includes polyparaphenylene benzobisoxazole (PBO) fibers<sup>79</sup>, polypropylene (PP) fibers<sup>103-105</sup> and polyethylene (PE) fibers.<sup>106-109</sup> All these fibers show an extraordinarily high chemical stability and therefore a highly inert fiber surface.<sup>69</sup> For the sake of completeness, however, it should be mentioned that concrete enriched with short fibers, e.g., polyvinyl alcohol (PVA), PP or E-glass fibers, are utilized in order to reduce crack formation and propagation as a result of concrete shrinkage, temperature effects, component stress and fatigue.

Short fibers, such as PP, PVA, high-density polyethylene (HDPE), AR glass, E-glass and steel fibers, in addition to the cementitious matrix contribute to enhancing the mechanical properties of concrete components, such as tensile strength, fracture toughness, resistance to fatigue, impact and thermal shock as well as flexural strength by forming a multiple crack formation.<sup>110-112</sup> Short fibers with their finite appearance are randomly oriented and supposed to be uniformly distributed throughout the concrete matrix, enhancing the tensile strength of the concrete component, even though they are not able to resist tensile stress to the same extent as endless fibers.<sup>69</sup> Therefore, in facade elements, sandwich components and very thin and slender concrete parts, appropriated short fibers are added to limit the crack width.<sup>14</sup> With regard to the increasing demand for sustainable solutions, natural fibers gain in importance for reinforcement materials in cementitious concrete<sup>110</sup>, such as hemp fibers<sup>113</sup>, flax fibers<sup>114-116</sup>, jute fibers<sup>117,118</sup>, sisal fibers<sup>119</sup>, cellulose fibers<sup>120</sup> and coconut coir fibers<sup>121,122</sup>, whereby coconut coir fibers have the strongest resistance to degradation in alkaline environments among all natural fibers.<sup>123</sup>



## 2.2. Impregnation materials

In the field of impregnation materials for textile reinforcement structures for concrete applications, there are two substantial chemical categories: impregnation agents based on polymers, such as thermosetting or thermoplastic matrices and thermoplastic elastomers, as well as mineral-based matrices, as shown in Table 2.2.1. Related to the construction industry, impregnation is defined as a homogeneous soaking of liquid impregnation material into the roving to achieve an optimal load transfer from outer to inner filaments.

The functions of impregnation treatments are to increase the bond strength and durability of reinforcing fiber materials in cementitious concrete matrices.<sup>124-127</sup> In addition, the impregnation material ensures that the structural geometry can be maintained for the fiber orientation, thus improving the handling properties during the processing and protecting the textile reinforcement from external factors during transportation or processing.<sup>125</sup> However, these advantages only appear if the impregnation material has homogeneously and fully infiltrated the fiber bundle, ensuring enhanced bonding between inner and outer filaments as well as between the entire roving and the surrounding concrete matrix.<sup>125</sup> Thus, an enhanced force transmission between filaments can be achieved compared to yarns without impregnation.<sup>128</sup> Furthermore, the impregnation stabilizes the textile formation along with improving the ease of application of textile reinforcement structures during the production processes. Ultimately, reinforcement fibers can sustain higher tensile forces so that their load capacity increases.<sup>129</sup>

**Table 2.2.1: Properties of selected impregnation materials for textile-reinforced concrete application<sup>130-143</sup>**

Impregnation category	Impregnation subcategory	Impregnation material	Glass transition temperature in °C	Processing temperature in °C
<b>Impregnation based on polymers</b>	Thermosetting matrix	Epoxy resin	81 – 225	18 – 180
	Aqueous dispersion	Based on acrylate	13 – 39	150
		Based on polystyrene	-5 – 33	150 – 160
		Based on styrene-butadiene	-8 – -5	130 – 160
		Based on polyurethane	< -30	120
<b>Impregnation based on minerals</b>	Mineral-based matrix	Granulated blast furnace slag	up to 500 <sup>a</sup>	20

<sup>a</sup> In case of a mineral-based impregnation material the assessment basis is the temperature of usability.

Polymer-based coatings can be divided into aqueous polymer dispersions with thermoplastic solids – for instance acrylate, polystyrene, styrene-butadiene rubber or ethyl acrylate – and thermosetting matrices, such as epoxy resin.<sup>141</sup> Recent investigations show the high potential of mineral-based coatings particularly with regard to thermal capacity, minimizing the deterioration of commonly used polymer-based impregnations while also decreasing the load-bearing properties under elevated temperatures.<sup>144-147</sup> Other exceptional approaches enhancing adhesive bonding between filaments involve the prepreg technology, whereby fibers are pre-impregnated with an unconsolidated thermoset matrix, and the hybrid yarn (commingled yarn) technology.<sup>148-150</sup>

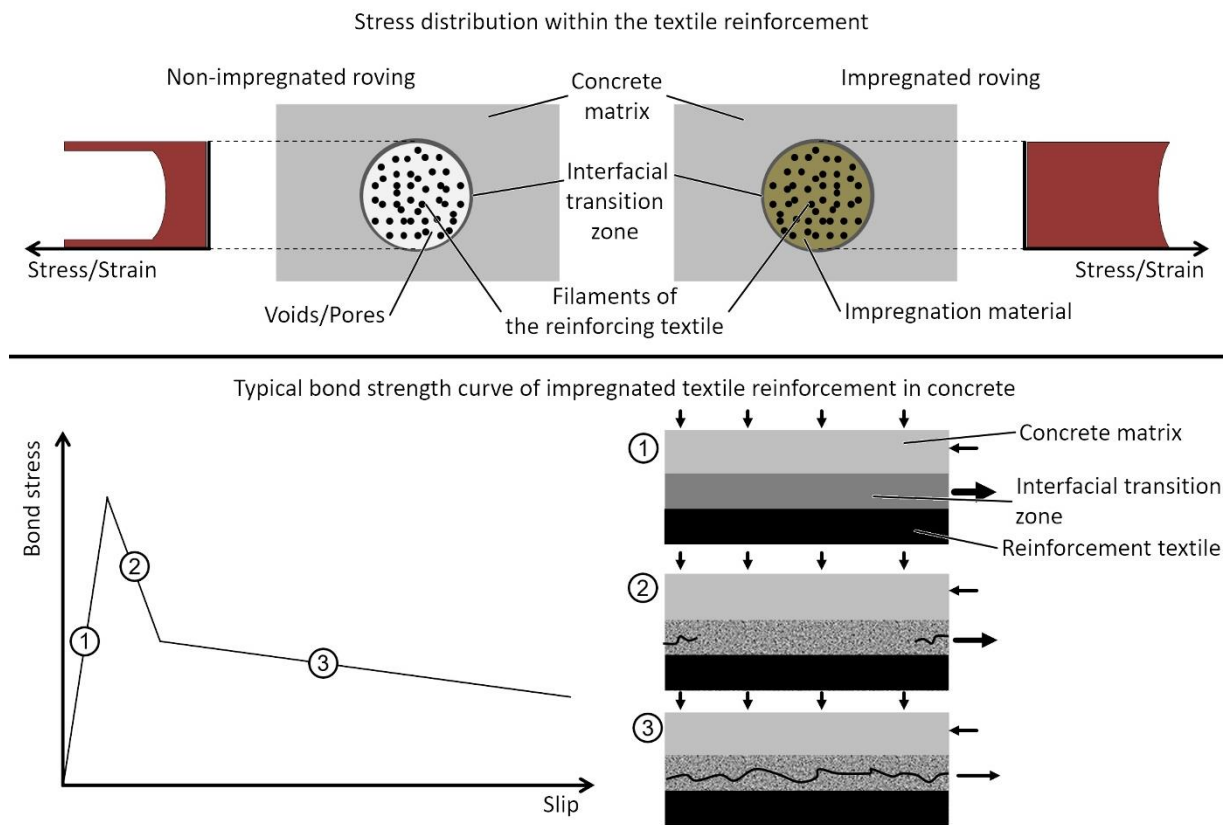
### 2.3. Interfacial transition zone

Traditional steel reinforcement bars are usually connected to the concrete matrix by mechanical interlocking achieved by a tailored surface profiling, e.g., using ribbed steel. The load is induced into the steel reinforcement at the steel ribs and distributed through the steel bar, which is made of a single, solid and isotropic material.<sup>151</sup> Modelling of the bond strength of steel-reinforced concrete has been researched for decades and an international standard has been established.<sup>152</sup>

In case of textile reinforcements, the load induction from concrete to reinforcement differs from steel reinforcements in two key areas. First, the textile reinforcement is not made from a singular solid material. Textile reinforcements consist of hundreds to thousands of individual anisotropic filaments. Only the outermost of those filaments are in direct contact with the surrounding concrete matrix, since the concrete is too coarse to penetrate into the textile reinforcement.<sup>153</sup> The inner filaments are not in direct contact with the concrete matrix and load induction into these filaments is subject to a second, inner load induction. The ratio of inner to outer filaments highly depends on the thickness and shape of the textile reinforcement.<sup>154</sup> Second, for textile reinforcements, in addition to mechanical interlocking, load induction by substance bond and by frictional bond are relevant.<sup>151</sup> The type of bond that is most relevant depends largely on the type of textile reinforcement.

For 1D textile reinforcements, mechanical interlocking plays a very important role, since 1D textile reinforcements closely resemble the traditional steel reinforcement bars concerning in size dimension and often sport a tailored surface profiling enabling mechanical interlocking.<sup>68,155</sup> For 2D and 3D textile reinforcements, substance bond and frictional bond are more important than mechanical interlocking, since the surface of these textiles is macroscopically comparatively flat and does not allow for significant mechanical interlocking.<sup>151</sup>

In case of non-impregnated textiles, which are only used in edge cases, most of the load is induced via frictional bond. Depending on the fiber material, some substance bond might be achieved (e.g., with PVA<sup>156</sup>), but most fiber materials do not form a significant substance bond with the concrete matrix.<sup>151</sup> This frictional bond is comparatively weak and leads to low failure loads. In addition, uncoated textiles usually fail with a so-called pull-out failure, in which the load is not transferred to the inner filaments of the roving and only the outer filaments carry the load.<sup>157</sup> Impregnation of the textile reinforcements allows for an increased substance bond of the reinforcement with the surrounding concrete matrix as well as for a better load transfer to the inner filaments of the reinforcement.<sup>141,157</sup> If sufficiently stiff impregnation materials are used, some measure of mechanical interlocking can be achieved, further increasing the bond strength.<sup>158</sup> This can also be achieved by adding a sand coating to the outside of an impregnated textile.<sup>100</sup> Figure 2.3 shows the load transfer in coated and uncoated textiles.



**Figure 2.3: Interfacial transition zone of non-impregnated and impregnated textile reinforcements for concrete (top: difference in stress distribution within the roving following Cherif<sup>159</sup>; bottom: typical bond strength curve of impregnated textile reinforcements in concrete following Lorenz<sup>157</sup>)**

Based on the models used for the bond behavior of steel reinforcement, adjusted models for textile reinforcements have been developed. Richter et al. were able to show in experiments that multiple sectional linear ranges are a sufficiently precise description of the composite behavior.<sup>160,161</sup> Several different calculation and modelling methods for the bond behavior of textile reinforced concrete exist, which currently require complex tests for calibration.<sup>162–165</sup>

In experimental testings, Wendler et al.<sup>166</sup> have investigated the mechanical characteristics of selected impregnated reinforcement textiles, especially of non-crimp fabrics (see section 3.2), that find mostly application in construction. Experimental testing results show tensile strength of up to 3,500 MPa for carbon-fiber non-crimp fabrics with impregnation based on polymers.<sup>166</sup>

In addition, Valeri et al. investigated the bond behavior of TRC using non-crimp fabrics. The influence of different parameters was investigated within the experimental plan, namely: the influence of certain impregnation types, the amount of longitudinal and transversal reinforcement and the concrete cover. Experimental results of tested tensile TRC specimen show an ultimate nominal roving stress in a range of 1,000 to 1,600 MPa depending on reinforcement type and reinforcement ratio.<sup>167</sup> Furthermore, Valeri et al. found that the tensile failure of all TRC specimen tested arises without any apparent warning sign and in a brittle manner.<sup>167</sup>

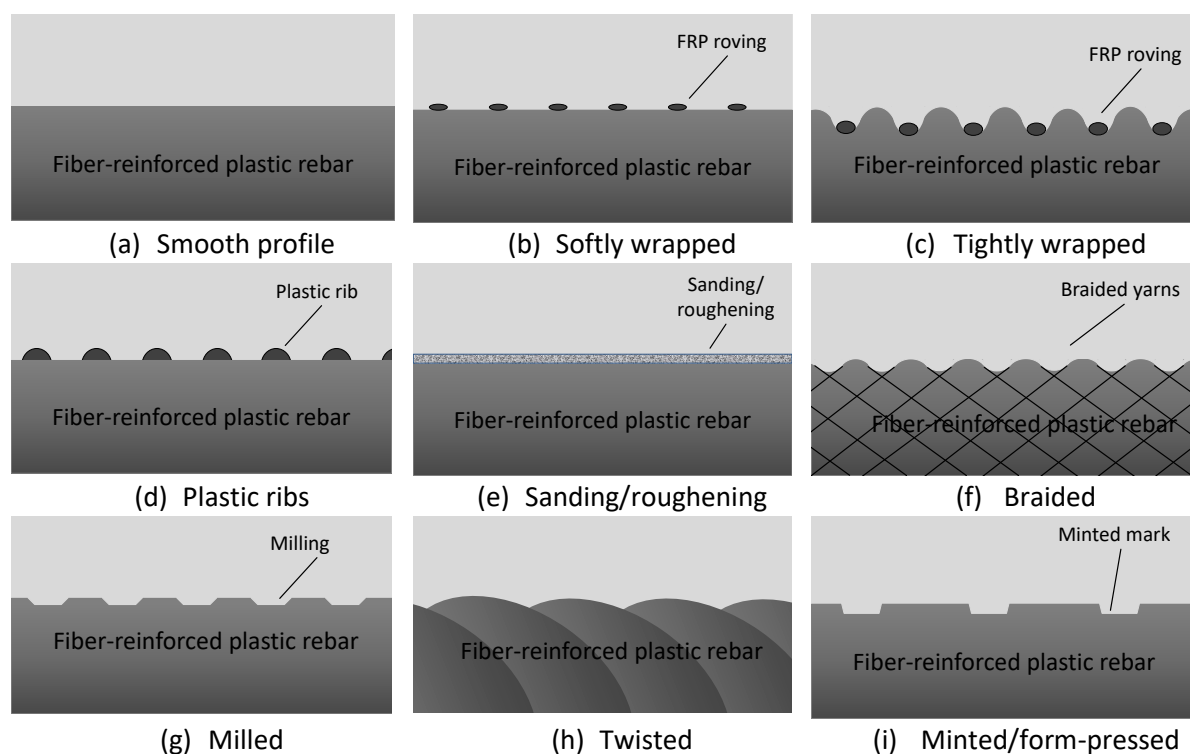
### 3. Textile reinforcement structures for construction applications

This chapter presents an overview of the wide range of common textile reinforcement structures already in use for concrete applications in the construction industry. The classification of these manifold textile reinforcement structures into one-dimensional (1D), two-dimensional (2D) and three-dimensional (3D) topologies enables a clear allocation according to their main reinforcement direction(s). New developments with a focus on robot-based manufacturing technologies and novel textile technologies currently under development are addressed in this section. In terms of fiber materials, this chapter is focused on reinforcements using carbon, AR glass and basalt fibers as they are the most commonly used materials. Within the comparatively new sector of non-metallic textile reinforcements for concrete components, standards are yet to be established so that currently, various textiles are employed for different applications. Nonetheless, a few types of textile reinforcement structures play a key role and are more commonly used than others. In general, textile reinforcement structures that are related to common steel reinforcement structures are very frequently used. Steel rebar is substituted by fiber-reinforced plastic rebar, while steel mats are substituted by 2D grid-like fabrics, which are either warp-knit or leno-woven. Since 2016, the first national technical approval published by Deutsches Institut für Bautechnik has universally regulated the procedure for reinforcing concrete with carbon-fiber warp-knitted reinforcement mats, which are bi- or multiaxial grids with regular orientation.<sup>168</sup> These reinforcement textiles in addition to other types are described in more detail below.

#### 3.1. 1D textile reinforcement structures

The term 1D textile reinforcement refers to reinforcing bars – or simplified just rebars – based on fiber composite material with one preferred reinforcement direction.<sup>169</sup> The international application of rebars proves the element's potential of significantly increasing the tensile strength of concrete components.<sup>170</sup> Bridge constructions with highly stressed plates caused by deicing salt<sup>171</sup>, such as the Shinmiya Bridge<sup>172</sup> in Japan and the Bridge Street Bridge<sup>173</sup> in the United States of America (USA), emphasize the international application field of 1D textile reinforcement topologies.

There have been comprehensive investigations into the tensile and bond-bearing behavior of carbon reinforcement mats in recent years. That is not the case for reinforced bars though, whose bond-bearing behavior is yet to be investigated in detail. Figure 3.1.1 illustrates a schematic overview of various kinds of rebars with varying surface finishes as a result of different manufacturing processes. Profiled rod-shaped fiber-reinforced plastic bars have to master the significant challenge of ensuring the transfer of (tensile) loads from external component stress on concrete to the reinforcement structures. In this context, the bond behavior is considerably influenced by the individual composite components – i.e., reinforcement fibers and matrix material – as well as the surface profile.



**Figure 3.1.1: Categorization of profiled textile reinforcement topologies such as fiber-reinforced plastic (FRP) rebars following Flemming et al.<sup>174</sup>**

As shown in Figure 3.1.1, different manufacturing technologies can be used to increase the bond behavior by means of surface profiling.<sup>175</sup> Apart from the straight and smooth (a) 1D textile reinforcement structure, there are various types of postprocessed elements. Essential manufacturing methods for profiling include: soft (b) and tight wrapping (c)<sup>175</sup>, adding polymeric ribs (d), sand-coating (e)<sup>175</sup>, braiding (f)<sup>176</sup>, milling (g)<sup>175</sup>, twisting (h)<sup>175</sup> and minting/form-pressed (i).<sup>175</sup> In addition, profiled carbon yarns with an altering tetrahedral cross-section geometry, which are reshaped in freshly impregnated condition, can also be taken into consideration for substantial 1D reinforcement structures.<sup>177</sup>

Another new development in the area of 1D textile reinforcement structures are carbon fiber tapes. These tapes are spread rovings, and since the spreading process increases the contact area between fiber and concrete, subsequent coating processes are usually no longer required. Scheurer et al. report increases in bending strength of up to 125 % for tapes with a spreading factor of 2.2 compared to TRC beams reinforced with unspread rovings.<sup>178</sup>

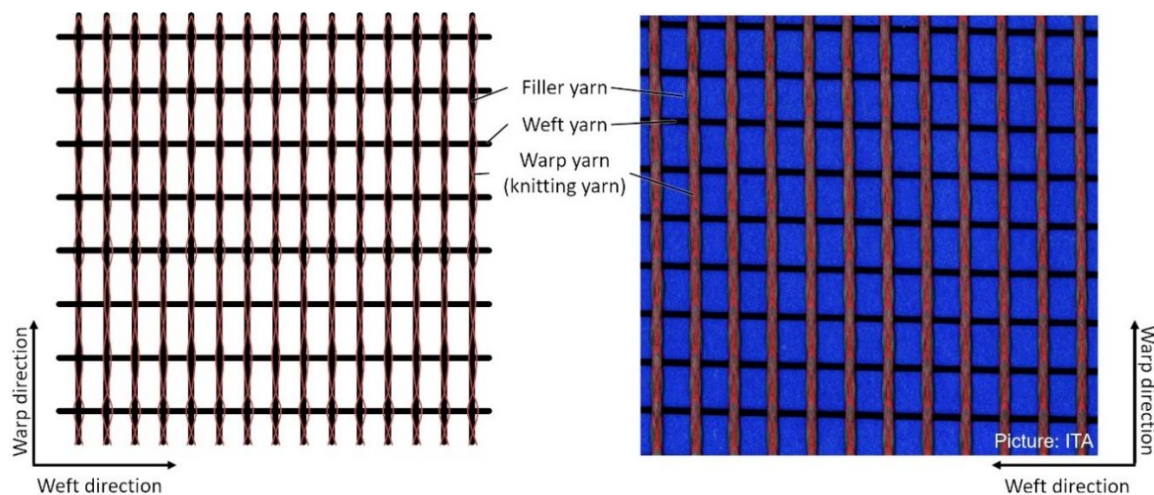
### 3.2. 2D textile reinforcement structures

2D textile reinforcement structures offer reinforcement in multiple directions of a plane. Similar to conventionally used steel reinforcement grids, the main reinforcement directions of reinforcement textiles for concrete construction are usually perpendicular to each other. For the reinforcement of concrete, three types of reinforcement structures produced by means of textile machine technology are relevant in academia and industrial applications: grid-like non-crimp fabrics (NCF), grid-like woven fabrics and weft-knitted textiles.<sup>11,179,180</sup> These textiles, their production processes and their design are discussed in this section.

### 3.2.1. Grid-like non-crimp fabrics (NCF)

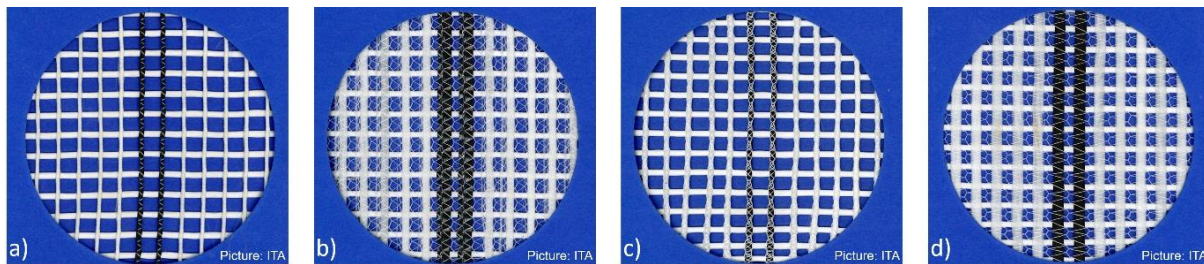
Grid-like NCFs are the most common reinforcement textiles used for concrete construction.<sup>70</sup> These textiles are produced using a warp-knitting process with a knitting thread connecting multiple layers of reinforcing fibers.<sup>181</sup> These reinforcing fibers are laid on top of each other and are, unlike fibers in woven fabrics, not crimped, leading to the designation “non-crimp fabric”. Since the reinforcing fibers are not crimped, NCFs offer higher elongation stiffness compared to traditional fabrics.<sup>70,72</sup>

For applications in concrete reinforcement, the textile needs to be embedded in the concrete matrix, requiring the concrete to penetrate through the textile. Since concrete consists of aggregates with a size of several millimeters, large gaps in the textile are necessary. For example, in the case of the textile specified for the German national technical approval Z 31.10-182, the distances between reinforcing fibers are 12.7 mm in weft direction and 14–16 mm in warp direction.<sup>168</sup> As a general rule, the minimal gap opening needs to be three times the size of the largest aggregate in the concrete mixture to prevent a filter effect during concreting.<sup>20</sup> These gaps are realized using warp-knitting processes, enabling the precise production of grid-like textiles with defined spacing between the reinforcing fibers. The warp-knitting processes are either course-oriented or non-course-oriented. During a course-oriented production process, reinforcing yarn distance and stitch length coincide so that the knitting needle does not penetrate through the reinforcing fiber, but produces the loops around it.<sup>72</sup> Most grid-like NCFs used for concrete reinforcement are biaxial, meaning they consist of reinforcement fibers in production direction (0°, filler yarn) and perpendicular to the production direction (90°, weft yarn). The basic structure and an example of a biaxial grid-like NCF as commonly used for concrete reinforcement are shown in Figure 3.2.1.1 below. Hausding et al. also developed an extended warp-knitting process enabling the production of symmetrical, multilayered biaxial NCFs (e. g., fabrics with a layer build-up of 0°/90°/0°).<sup>182</sup>



**Figure 3.2.1.1: Structure of grid-like non-crimp fabric and example picture**

Apart from the material selection, the most important parameters for the production of grid-like NCF for concrete reinforcement are the knitting parameters, especially stitch type and stitch length.<sup>183</sup> Increased stitch length leads to increased shear resistance of grid-like NCF<sup>183</sup> and also results in an increased mechanical performance of TRC elements.<sup>104</sup> While the number of possible stitch types is practically unlimited, especially on modern, electronically controlled machines, several stitch types are especially important, including pillar, tricot, counterlaid tricot and plain. These stitch types are shown in Figure 3.2.1.2 below.



**Figure 3.2.1.2: Different stitch types common in grid-like NCF for construction applications. [a] pillar stitch [b] tricot stitch [c] counterlaid tricot stitch [d] plain stitch**

The stitch type influences various properties of the reinforcement textile and resulting TRC structure, starting with the shape of the cross section of the reinforcing fibers. This in turn affects the sleeve area in contact with the concrete matrix, which determines the load transfer from concrete to textile, ultimately influencing the mechanical performance of the reinforced concrete elements.<sup>184</sup> Several studies have reported increased pull-out strength and mechanical performance of specimens reinforced with grid-like NCF with wider stitch types, such as tricot or plain.<sup>183,185–187</sup> In all these studies, the textiles were used without additional coating. Perry et al. reported similar results for non-impregnated textiles, but different results for impregnated textiles.<sup>184</sup> In the case of impregnated textiles, stitch types with rounder cross sections, such as pillar or counterlaid tricot, seem to be beneficial.<sup>184</sup>

Grid-like NCF can be impregnated in offline or online processes. In offline processes, the textile is impregnated in an additional production step on a separate machine, while an online process integrates the impregnation into the textile production process.<sup>125</sup> A machine concept for the online impregnation of grid-like NCF was initially described and evaluated by Köckritz et al.<sup>188,189</sup> and further developed by Hahn.<sup>125</sup> Online impregnation of grid-like NCF is nowadays an established process in the textile industry for the production of concrete reinforcement textiles. An evaluation of impregnation parameters by Hahn et al. proved an increase in tensile strength of impregnated grid-like NCF of up to 10 % compared to standard parameters used in the industry.<sup>190</sup>

In an effort to develop highly drapable reinforcement textiles, Pidun investigated biaxial grid-like NCF with variable stitch types along the production length to enable bending of the textiles at specific locations to allow for the shaping of TRC elements during the curing of the concrete.<sup>191</sup> Similarly, Dittel et al. developed a reinforcement textile based on grid-like NCF with reinforcement only in weft direction utilizing flexible knitting yarns made of silicone to produce highly drapable textiles for doubly curved facade elements.<sup>192</sup>

An additional advantage for the production of grid-like NCF is the possibility to replace selected fibers in the structure. This enables the production of textiles with special properties in select areas. For example, replacing selected fibers in a glass textile with carbon fibers allows the use of these carbon fibers as sensor material.<sup>193</sup> Changes in the electrical conductivity of carbon fibers can be detected and allow their application as sensors in structural health monitoring, detecting strain and cracking<sup>194–197</sup> as well as water intrusion.<sup>198,199</sup>

Another development for grid-like NCF for construction applications based on multiaxial warp-knitting technology is the development of loop-shaped anchoring points at both sides of the textile done by Rittner et al.<sup>200</sup> The loop-shaped anchoring points reduce anchoring lengths to 100 mm or less, enabling a reduction of overlapping lengths in large structures, where multiple textiles are required, by more than 75 %.

Grid-like NCF can also be produced in an alternative production process eschewing warp-knitting, as reported by Hahn et al.<sup>201</sup> In this process, the layers of the textile are placed on top of each other and

bonded using adhesives or impregnation processes. Initial results show an increase in breaking force at the bond points of 4–30 % compared to conventional, warp-knit grid-like NCF.<sup>201</sup>

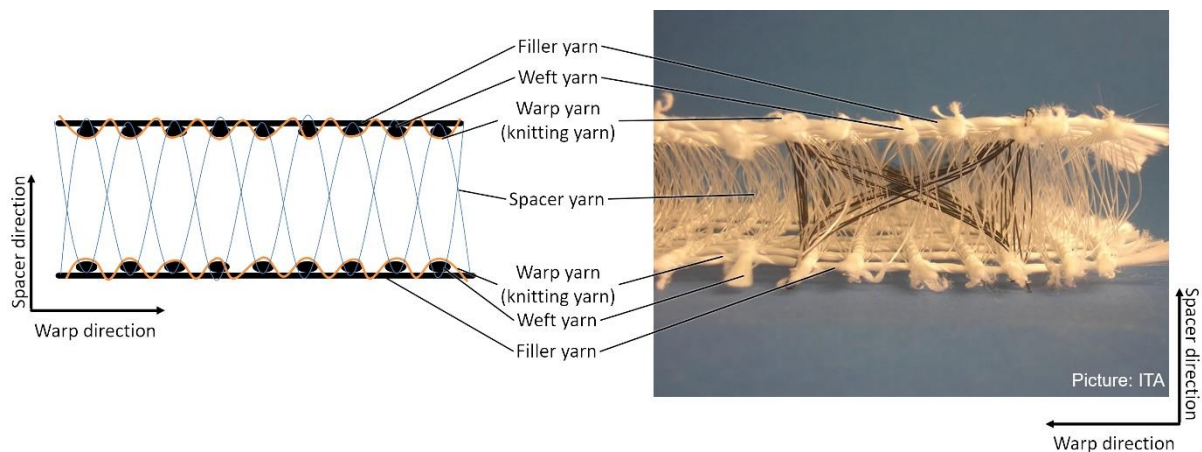
The production of TRC elements often requires shaped reinforcements in addition to flat reinforcement mats, for example L-shaped reinforcements in corner areas. The production of such 3D-shaped reinforcements is usually done in discontinuous processes, where the textile is coated, shaped and then cured in distinct steps on different machines.<sup>202,203</sup> A newly developed process by Hahn et al. enables the continuous in-line impregnation, shaping and curing of grid-like NCF.<sup>204–207</sup>

In addition to the commonly used biaxial grid-like NCF, the production of multiaxial grid-like NCF is feasible.<sup>208</sup> Based on such bi- and multiaxial grid-like NCFs, Sankaran et al. developed a numerically controlled delivery and doffing system for the multiaxial warp-knitting technology to produce grids with variable warp yarn lengths, which enables the production of 2D reinforcement textiles adapted for specific curved 3D shapes, such as the shells of a pavilion.<sup>74,209–211</sup>

### 3.2.2. Spacer fabrics

Warp-knit spacer fabrics are produced using double-bar raschel machines producing two layers of a warp-knit textile connected by spacer yarns.<sup>212</sup> The individual layers are similar to the 2D, grid-like NCFs described above and consist of reinforcement yarns in 0° and 90° directions as well as a knitting yarn connecting them. The distance between the layers can be adjusted not only between textiles, but also on the fly during production.<sup>213</sup> The basic structure and an example of a warp-knit spacer fabric as used for concrete reinforcement are shown in Figure 3.2.2.1 below.

While spacer fabrics offer a textile with a 3D yarn architecture and are often referred to as 3D textiles, the spacer yarns are comparatively thin polymer yarns that do not offer significant reinforcement for concrete applications. Therefore, spacer fabrics offer two layers of 2D reinforcement.



**Figure 3.2.2.1: Basic structure and example of a warp-knitted spacer fabric as used for concrete reinforcement**

Roye et al. analyzed different warp-knitted spacer fabrics for concrete applications and compared their resistance to compressive forces.<sup>213,214</sup> They reported a decrease in compression resistance with a decreasing spacer yarn angle<sup>213</sup> and with decreasing amount of spacer yarn<sup>214</sup>, as well as a dependency of compression resistance on spacer yarn material.<sup>214</sup> Haik et al. evaluated the suitability of spacer fabrics for concrete reinforcement and found them to be highly beneficial.<sup>215</sup> Depending on the type of fabric construction, they found the performance of spacer fabrics to be highly anisotropic.<sup>215</sup> Similarly, El Kadi et al. compared the performance of spacer fabrics and equivalent 2D textiles, revealing that there is no difference in tensile strength of TRC elements, but a higher



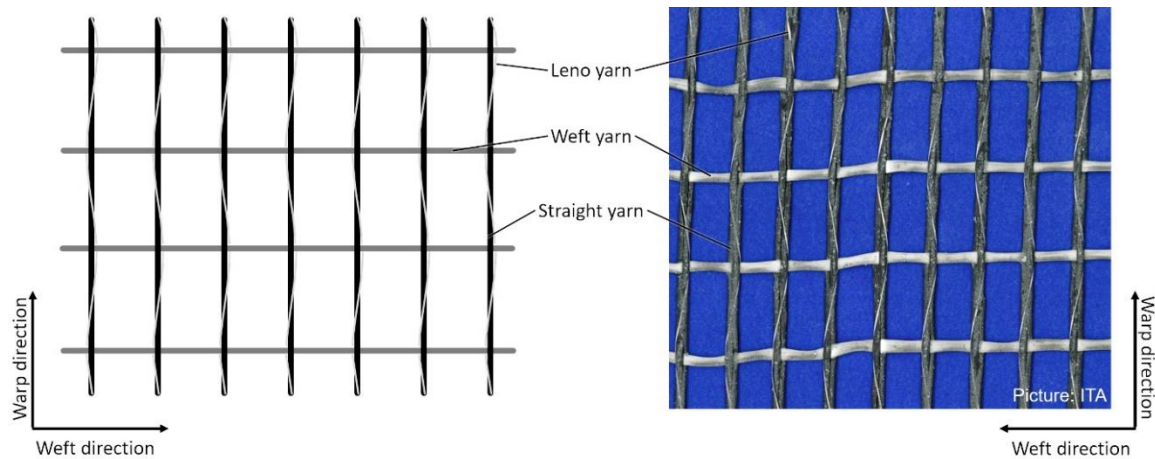
bending strength when using spacer fabrics.<sup>216</sup> Spacer fabrics are also employed in Concrete Canvas, a special type of geosynthetic cementitious composite mat consisting of a spacer fabric filled with concrete powder, which is hardened on-site by adding water.<sup>217</sup> Han et al. investigated different spacer fabric geometries and their applicability for Concrete Canvas, suggesting the use of a solid outer layer.<sup>218</sup> Han et al. also analyzed the influence of spacer fabric geometry on the drying shrinkage of Concrete Canvas, with drying shrinkage mainly depending on the spacer yarns.<sup>219</sup> Li et al. investigated different spacer fabric geometries used in Concrete Canvas and developed a lattice model predicting the tensile behavior of Concrete Canvas based on the geometry of the 3D spacer fabric.<sup>220</sup> Recent development efforts focused on specialized spacer fabrics easing the combination of multiple textiles during construction. By reducing the distance between the reinforcement layers of the spacer fabric at the sides of the textile, multiple textiles can be overlapped without increasing the resulting thickness of the element.<sup>221</sup>

### 3.2.3. Grid-like woven fabrics

Weaving has been used to produce fabrics for more than 5,000 years and is the most common production method for fabrics today.<sup>72</sup> Woven fabrics consist of warp and weft threads which are interlaced during production, usually at right angles.<sup>222</sup>

Woven fabrics were among the first textiles considered as reinforcement textiles for concrete in the 1990s. For example, Peled et al. analyzed plain woven fabrics made from polyethylene monofilament yarns and reported an improvement in textile-concrete bond (compared to straight yarns) due to the crimped structure of the textile providing mechanical anchoring.<sup>223</sup> They also determined an optimal yarn density above which the concrete matrix cannot penetrate into the textile, reducing mechanical performance.<sup>223</sup> Similarly, Perez-Pena and Mobasher used woven polypropylene and AR glass meshes as effective reinforcements for concrete.<sup>224</sup>

While initial analyses used very fine concrete mixtures or cementitious matrices, later concrete developments with coarser aggregates required larger mesh openings to enable concrete penetration into and through the textile reinforcement structure. Since the maximum mesh opening is limited in conventional woven textiles, leno-woven textiles are employed to overcome these geometrical limitations. With leno-woven fabrics, at least two warp yarn systems are employed: straight and leno yarns.<sup>225</sup> In contrast to standard woven textiles, warp and weft yarn are not always interwoven, but can be connected via the leno yarns.<sup>226</sup> This enables the production of a woven textile with straight reinforcement yarns in warp and weft direction.<sup>226</sup> Additionally, due to this structure, woven fabrics with low warp and weft densities and therefore large mesh openings can be produced.<sup>225,227</sup> The basic structure and an example of a grid-like woven fabric as used for concrete reinforcement are shown in Figure 3.2.3.1 below. Grid-like woven fabrics were used in TRC in several studies, in which they were found to be effective reinforcement textiles.<sup>228–230</sup>



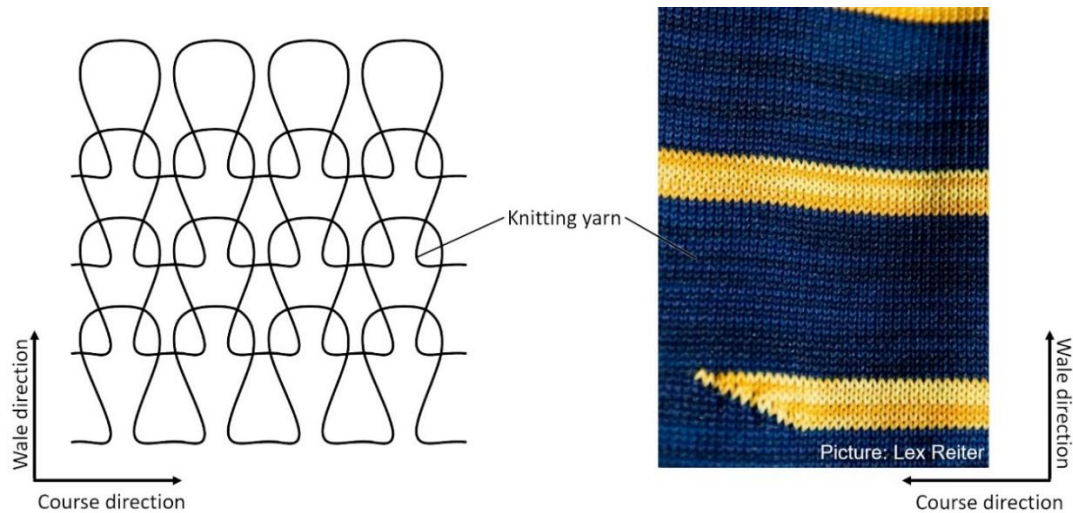
**Figure 3.2.3.1: Basic structure and image of a grid-like woven fabric**

Compared to conventional leno-weaving machines, machines for the production of grid-like woven fabrics require some alterations. Hausding et al. exchanged several key machine components (e.g., thread heddles / warp beams) to enable the processing of high-performance fiber materials like carbon and AR-glass.<sup>228</sup> Lenz et al. increased the amount of warp-yarn twist that can be introduced on leno-weaving machines as well as production speeds, enabling cheaper textiles with larger mesh openings.<sup>231</sup> And Weise et al. further modified the weaving machines to enable the processing of coarse high-performance fibers (> 2,400 tex) and to reduce the crimp of the reinforcing warp yarn.<sup>225</sup>

Another application of woven fabrics for concrete reinforcement is the fabric formworks suggested by Brennan et al.<sup>232</sup> Woven textile structures can be used as lost formwork during concrete production, where they are either employed only as a flexible formwork, enabling highly curved, nonlinear structures, or as formwork and reinforcement in one.<sup>232</sup>

### 3.2.4. Weft-knitted structures

Weft-knit fabrics are produced from one or several thread systems by stitch formation, meaning the threads are formed into loops and connected with adjacent loops.<sup>72</sup> Since this production process leads to a comparatively flexible textile with very small gap sizes, weft-knit textiles are an unusual choice for the pure reinforcement of hardened concrete. However, weft-knit fabrics can be employed in concrete construction for the reinforcement of fresh concrete. In that case, weft-knitted structures are used as stay-in-place formworks, also dubbed KnitCrete.<sup>66</sup> Figure 3.2.4.1 below shows the basic structure and an example of a weft-knit textile.



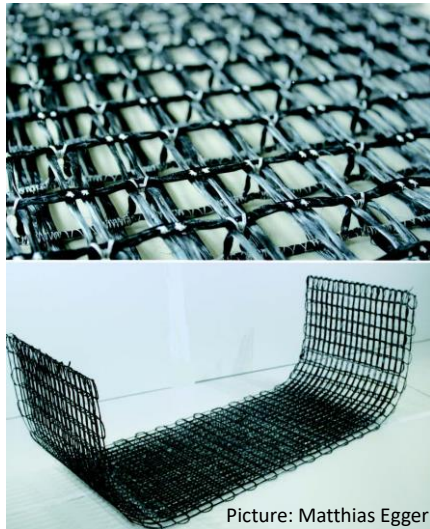
**Figure 3.2.4.1: Basic structure and image of a weft-knit fabric utilized to reinforce fresh concrete (KnitCrete<sup>66</sup>)**

Utilizing double-bed flat-knitting machines, Popescu et al. produced several stay-in-place formworks for concrete structures.<sup>66,233–236</sup> Using a double bed machine enables the production of a weft-knit textile with two sides for different purposes. While one side has an aesthetically pleasing design (color/structure), the other side is used for the inclusion of reinforcing cables by providing anchoring points and hooks.<sup>66</sup> The distance between the two sides of the textile is adjusted by means of balloons.<sup>66</sup>

### 3.3. 3D textile reinforcement structures

3D textiles as defined in this paper offer textile reinforcement in all three spatial dimensions. This type of reinforcement is comparatively rare and has so far only been investigated in a few research projects. In the case of most TRC applications, various 2D textiles are combined to produce a 3D reinforcement since the production of 3D textiles is comparatively expensive.

One possibility for 3D textile reinforcement are 3D concrete-filled fiber-reinforced plastic branchings, which can be produced using a newly developed technological braiding process obtaining triaxial braidings. The utilized radial braiding machine is used to manufacture branched, knot-like, 3D textile structures with altering knot geometries and appropriated surface coverages, whereby the focus is also on adding continuous stationary reinforcing threads with an axial alignment coinciding with the normal force direction.<sup>237</sup> In comparison to plain concrete specimens as reference, the generated concrete-filled fiber-reinforced plastic knot structures show an enhanced load-bearing capacity through load-adapted fiber arrangements inspired by natural role models.<sup>237</sup>



Picture: Matthias Egger

- (a) 3D reinforcement embroidery  
Institute for Design and Material Science  
University of Innsbruck (UIBK)



Picture: ITKE, University of Stuttgart

- (b) 3D reinforcement braiding  
Institute of Building Structures and Structural Design (ITKE)  
University of Stuttgart

**Figure 3.3.1: Non-metallic 3D textile reinforcement structures with strengthening function in all three spatial dimensions<sup>237,238</sup>**

Another possibility for the production of 3D reinforcement textiles involves technical embroidery. This process allows the controlled placement of yarns in any direction, enabling the production of load-adapted reinforcement.<sup>238</sup> The reinforcement yarns are embroidered onto a soluble carrier textile, which is subsequently removed. The structure is then spread out, coated and consolidated. Similar to spacer fabrics, the resulting textiles consist of two layers of reinforcement placed at a defined distance to each other. However, the distance is not controlled by using an additional yarn system, but by the reinforcement yarns themselves.<sup>238</sup>

#### 4. New developments in robot-supported manufacturing technologies for construction applications

Textile-reinforced concrete is gaining attention for its potential for producing geometrically sophisticated and complex structures in research and the construction industry.<sup>239–241</sup> Hence, its scope is increasingly being extended so that even geometrically sophisticated three-dimensional (3D) concrete components with free-formed outer shapes are reinforced with state-of-the-art manufacturing processes, e.g., the previously mentioned knitting, weaving and warp-knitting processes. However, in most cases, the production of these kinds of reinforcement structures is associated with a high level of waste, especially when reinforcement shows a complex, highly branched inner structure with gradual contours. The conventional textile manufacturing processes cannot offer a flexibly adaptable machine technology to easily modify the main textile reinforcement structure toward the preferred direction without time-consuming machine and process modifications as well as without rework.

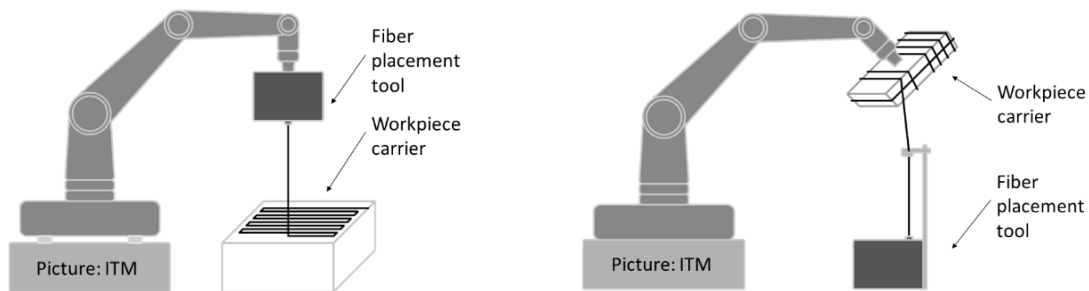
Therefore, special robot-based machine technology paves the way for novel resource-saving and cost-efficient textile reinforcement structures. Von Zuben et al. developed six-axis robot technology which is capable of producing planar and grid-like reinforcements using freshly impregnated carbon fiber heavy tow (CFHT).<sup>67</sup> Even though presently, planar structures and two-dimensional (2D) component geometries can already be realized and are applied for 2D stress states, this robot-supported technology constitutes a crucial bridge toward complex multi-branched reinforcement topologies.<sup>242–244</sup> This technology is characterized by the fact that the robot manipulates the fiber placement tool and the workpiece carrier is stationary, as shown in Figure 4.1 (a).

Furthermore, there are even robot-support manufacturing technologies enabling the production of 3D reinforcement topologies according to the definition given above in Section 3c – 3D textile reinforcement structures. The 3D coreless filament winding technique is a translative cross winding technology enabling the fabrication of 3D trusses for reinforcement utilization by Minsch et al.<sup>245–247</sup> Initially, this technology was developed for the production of automotive operating materials in energy-reduced manufacturing processes.<sup>248</sup> The producible carbon fiber reinforcement structures have mechanically high-performance properties, though containing the winding elements within the fiber-reinforced plastic structure for the rest of the component's life. This production technology is usable for truss-like reinforcement structures of any kind and suitable for producing reinforcement structures with a focus on concrete construction components. In this case, an industrial six-axis robot handles the CFHT, whereas the workpiece carrier is fixed and only the fiber placement tool is working. The translative cross-winding technology processes freshly impregnated fibers (thermosetting resin) to simple spatial structures with no gradual fiber orientation.

Another novel production technology by Michel and Mechtcherine et al. is the winding technique by means of a winding core, which realizes simple, rotationally similar and shell-like fiber structures with no gradual fiber orientation.<sup>71,249</sup> This technology uses pre-impregnated CFHTs and it is applicable for concrete parts with a low degree of complexity as reinforcement cages. The six-axis robot technology is characterized by manipulating the workpiece carrier, as the fiber placement tool remains dormant, as shown in Figure 4.1 (b).<sup>71</sup> Here the solid and fluid media are located on the ground, which enables the free guidance of the workpiece carrier with the impregnated fiber structure increasing the degrees of freedom of the robot.

The manufacturing technologies in Figure 4.1 form the basic technologies in the robotic production of textile reinforcement structures, with a process difference in terms of yarn impregnation and a difference in the manipulation of the tool and workpiece carrier. In addition, other robot-assisted

manufacturing processes exist for textile reinforcement structures, which are to be regarded as derivatives of the two basic technologies.



(a) Robot manipulates fiber placement tool  
Technische Universität Dresden, Germany

(b) Robot manipulates workpiece carrier  
Technische Universität Dresden, Germany

**Figure 4.1: Classified robot production technologies for manufacturing textile reinforcement structures for concrete construction application<sup>67,71</sup>**

A new approach of producing large-scale shell elements is the robotized production by means of collaboratively used robot systems, consisting of six-axis robots, drones and climbing robots (Research Pavilions; BUGA Fiber Pavilion 2019).<sup>250,251</sup> The manufactured 3D textile topologies have a membranous outer appearance exclusively using prepregs. Here, the workpiece carrier is fixed and the robots place the pre-impregnated fibers in gradual fiber orientation matching the load-adapted design approach of construction components. To date, this technology has been used for creative-architectural application within the construction industry rather than for the reinforcement of concrete. Even if this technology is currently applied to produce components with an architectural focus, the manufacturing principles can be analogically transferred to a production scheme for 3D textile reinforcement topologies with regard to concrete parts.

The robot-supported manufacturing technology needs to meet the requirement in order to provide 3D textile reinforcement topologies with spatial branchings and a load adapted fiber orientation. In particular, the enhanced flexibility to place fibers with the use of six-axis robots must be taken advantage of in order to produce highly complex fiber structures, for instance in the use of textile reinforcements for corner areas, reinforcement cages or load-adapted design components.

## 5. Conclusions

Since the 1990s, high-performance textile materials have been investigated for use in reinforcing concrete components and the industrial applications are steadily growing.<sup>252-257</sup> Various types of textile reinforcement structures exist, which can at the most basic level be divided into 1D, 2D and 3D structures. For 2D reinforcements, an additional distinction is made between 2D and 3D shape.

In conventional concrete structures, the concrete accounts for by far the largest share of the global warming potential. If this share can be reduced, the greatest effect on sustainability is achieved in the overall balance.<sup>9</sup> For that reason, the ambitions of the research and the industries involved are to substitute steel reinforcements for concrete applications with tailor-made technical textiles. So, the first national technical approval published to universally regulate the procedure for reinforcing concrete with carbon-fiber warp-knitted reinforcement mats in Germany can be seen as an interim success. Textile reinforced concrete (TRC) offers several advantages in comparison to steel-reinforced concrete, such as corrosion resistance, which has a positive effect on the longevity of the reinforced concrete component. In addition, concrete consumption is considerably reduced as a result, since the thick concrete cover that would otherwise protect the steel reinforcement against corrosion can be reduced. This, in turn, has a positive effect on the environment because carbon dioxide emissions are reduced due to the lower cement consumption. In addition, the possibilities of diverse and creative shaping can expand the architectural design scope when TRC components with low thicknesses in the range of one to five centimeters are used.

Meanwhile, almost all common textile technologies have been scientifically examined or industrially used to pave the way for the concrete reinforcement of technical textiles. Manufacturing technologies such as wrapping, braiding, twisting and spreading for 1D textiles, warp- and weft-knitting as well as weaving for 2D reinforcement structures, and braiding as well as embroidery for 3D textile structures have the ability to reinforce specific concrete components in the construction industry. The review shows that technical textiles with continuous and non-crimped fibers (e.g., non-crimp fabrics) have higher load-bearing potential for reinforcing concrete components than technical textiles with undulated fiber structures (e.g., woven and knitted fabrics). Possibly for this reason, technical textiles such as bi- and multi-axial fabrics (warp-knitting technology) have been more successful than warp-knit spacer fabrics, weft-knit fabrics and grid-like woven fabrics in industrial construction applications. Moreover, compared to the other technological textile manufacturing processes, the warp-knitting technology is significantly more productive regarding the production volume.<sup>69</sup> However, the full potential of technical textiles is not being fully exploited, as the currently used textile reinforcement structures predominantly reflect the steel reinforcements. There is more potential in TRC, especially for geometrically complex structures. The fibers need to be placed according to the main load direction of the final concrete component. Only if the fiber orientations correspond to the load direction the reinforcement is able to fully exploit its anisotropic material properties, especially the high tensile stiffness and strength. Potential utilization can be achieved in textile-reinforced concrete components by using load transfer mechanisms specifically in the area of non-straight trajectories or principal stress courses and consequently reducing local material usage due to reduced oversizing. Even highly productively produced conventional reinforcement textiles such as non-crimp fabrics can be postprocessed to generate load-adapted 3D textile reinforcement topologies. In order to meet the ever-increasing requirement for increasingly complex component contours in the construction industry as well as the demand for more efficiently produced and resource-saving textile reinforcement structures, further research is needed into innovative and flexible manufacturing technologies producing load-adapted 3D textile reinforcement structures.

Developed robot-supported textile manufacturing technologies can already produce 3D textile reinforcement topologies with the characteristic of a membranous structure. These highly flexible robotic manufacturing processes show the potential to produce novel and innovative design approaches for material-minimized concrete constructions. Further development is necessary to take full advantage of TRC by robotically manufactured, biologically inspired textile reinforcements with spatially branched structures and according to a load-adapted fiber orientation throughout the whole textile reinforcement structure.

Thus, a key strategy to tackle cement-related CO<sub>2</sub> emissions is to minimize the use of cement and the efforts resulting from component transport as well as to enhance the concrete components' longevity by realizing textile-based and resource-saving concrete construction approaches. Already these novel design methods within the construction industry along with the appropriate textile manufacturing processes for textile reinforcement topologies have a high potential to manage one of the main drivers of the greenhouse gas carbon dioxide: the excessive global production of cement.

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### Declaration of Conflict of Interests

The authors declare that there is no potential conflict of interest with respect to the research, authorship and/or publication of this article.



## References

1. European Commission. On Resource Efficiency Opportunities in the Building Sector. COM(2014) 445 final, Brussels, 1 July 2014.
2. European Commission. Communication from the Commission to the European Parliament, the Council, the European Economic and social Committee and the Committee of the Regions: Roadmap to a Resource Efficient Europe. COM(2011) 571 final, European Commission, Brussels, 20 September 2011.
3. Ruuska A and Häkkinen T. Material Efficiency of Building Construction. *Buildings* 2014; 4: 266–294.
4. Beyond Zero Emissions. *Rethinking cement: Zero carbon industry plan*. Fitzroy, Victoria: Beyond Zero Emissions Inc, 2017.
5. Scheerer S. Was ist Textilbeton? *BETON- STAHLBETONBAU* 2015; 110: 4–7.
6. Hegger J, Goralski C and Kulas C. Schlanke Fußgängerbrücke aus Textilbeton. *BETON- STAHLBETONBAU* 2011; 106: 64–71.
7. Laiblová L, Pešta J, Kumar A, et al. Environmental Impact of Textile Reinforced Concrete Facades Compared to Conventional Solutions-LCA Case Study. *Materials (Basel)* 2019; 12.
8. Scope C, Guenther E, Schütz J, et al. Aiming for life cycle sustainability assessment of cement-based composites: A trend study for wall systems of carbon concrete: Dresden Nexus Conference 2020-Session 4-Circular economy for building with secondary construction materials to minimise resource use and land use. *Civil Engineering Design* 2020; 2: 143–158.
9. Seifert W and Lieboldt M. Ressourcenverbrauch im globalen Stahlbetonbau und Potenziale der Carbonbetonbauweise. *Beton- Stahlbetonbau* 2020; 115: 469–478.
10. Stoiber N, Hammerl M and Kromoser B. Cradle-to-gate life cycle assessment of CFRP reinforcement for concrete structures: Calculation basis and exemplary application. *J CLEAN PROD* 2021; 280: 124300.
11. Triantafyllou T (ed). *Textile fibre composites in civil engineering*: Elsevier, 2016.
12. Peled A, Bentur A and Mobasher B. *Textile reinforced concrete*. London: CRC Press, 2017.
13. Reichenbach S, Preinstorfer P, Hammerl M, et al. A review on embedded fibre-reinforced polymer reinforcement in structural concrete in Europe. *CONSTR BUILD MATER* 2021; 307: 124946.
14. Afroughsabet V, Biolzi L and Ozbakkaloglu T. High-performance fiber-reinforced concrete: a review. *J MATER SCI* 2016; 51: 6517–6551.
15. Pakravan HR, Latifi M and Jamshidi M. Hybrid short fiber reinforcement system in concrete: A review. *CONSTR BUILD MATER* 2017; 142: 280–294.
16. Shaikh FUA, Luhar S, Arel HŞ, et al. Performance evaluation of Ultrahigh performance fibre reinforced concrete – A review. *CONSTR BUILD MATER* 2020; 232: 117152.
17. Wu H, Lin X and Zhou A. A review of mechanical properties of fibre reinforced concrete at elevated temperatures. *CEMENT CONCRETE RES* 2020; 135: 106117, <https://doi.org/10.1016/j.cemconres.2020.106117> (2020, accessed 3 December 2021).
18. Tatar J and Milev S. Durability of Externally Bonded Fiber-Reinforced Polymer Composites in Concrete Structures: A Critical Review. *POLYMERS-BASEL* 2021; 13.
19. Arnold RD, Bartl AMD, Eberhardt HD, et al. Bewehrtes vorgefertigtes Einzelbauteil. Patent application DD19820246779 19821230, DD, 1982.
20. Curbach M and Jesse F. Eigenschaften und Anwendung von Textilbeton. *BETON- STAHLBETONBAU* 2009; 104: 9–16.
21. Hegger J and Voss S. Investigations on the bearing behaviour and application potential of textile reinforced concrete. *ENG STRUCT* 2008; 30: 2050–2056.

22. Koutas LN, Tetta Z, Bournas DA, et al. Strengthening of Concrete Structures with Textile Reinforced Mortars: State-of-the-Art Review. *J COMPOS CONSTR* 2019; 23: 3118001.
23. Gagg CR. Cement and concrete as an engineering material: An historic appraisal and case study analysis. *ENG FAIL ANAL* 2014; 40: 114–140.
24. Lohmeyer GCO. *Stahlbetonbau: Bemessung, Konstruktion, Ausführung ; mit 194 Tafeln und zahlreichen Beispielen*. 5., neubearbeitete und erweiterte Auflage. Stuttgart: Teubner, 1994.
25. Deutsches Institut für Normung e.V. 488-1. DIN 488-1:2009-08.
26. Deutsches Institut für Normung e.V. 488-2. DIN 488-2:2009-08.
27. Deutsches Institut für Normung e.V. 488-3. DIN 488-3:2009-08.
28. Deutsches Institut für Normung e.V. 488-4. DIN 488-4:2009-08.
29. Carozzi FG, Poggi C, Bertolesi E, et al. Ancient masonry arches and vaults strengthened with TRM, SRG and FRP composites: Experimental evaluation. *COMPOS STRUCT* 2018; 187: 466–480.
30. Harajli M, ElKhatib H and San-Jose JT. Static and Cyclic Out-of-Plane Response of Masonry Walls Strengthened Using Textile-Mortar System. *J MATER CIVIL ENG* 2010; 22: 1171–1180.
31. Leone M, Aiello MA, Balsamo A, et al. Glass fabric reinforced cementitious matrix: Tensile properties and bond performance on masonry substrate. *COMPOS PART B-ENG* 2017; 127: 196–214.
32. Curbach M, Hauptenbuchner B, Ortlepp R, et al. Textilbewehrter Beton zur Verstärkung eines Hyparschalentragwerks in Schweinfurt. *BETON- STAHLBETONBAU* 2007; 102: 353–361.
33. Erhard E, Weiland S, Lorenz E, et al. Anwendungsbeispiele für Textilbetonverstärkung. *BETON- STAHLBETONBAU* 2015; 110: 74–82.
34. Rempel S, Erhard E, Schmidt H-G, et al. Die Sanierung des Mariendomedaches in Neviges mit carbonbewehrtem Spritzmörtel. *BETON- STAHLBETONBAU* 2018; 113: 543–550.
35. Schladitz F, Lorenz E, Jesse F, et al. Verstärkung einer denkmalgeschützten Tonnenschale mit Textilbeton. *BETON- STAHLBETONBAU* 2009; 104: 432–437.
36. Weiland S, Schladitz F, Schütze E, et al. Rissinstandsetzung eines Zuckersilos. *Bautechnik* 2013; 90: 498–504.
37. Adam V, Bielak J, Dommies C, et al. Flexural and Shear Tests on Reinforced Concrete Bridge Deck Slab Segments with a Textile-Reinforced Concrete Strengthening Layer. *MATERIALS* 2020; 13.
38. Holschemacher K. Application of Textile Reinforced Concrete in Precast Concrete Industry. *IOP Conference Series: Materials Science and Engineering* 2020; 753: 42086.
39. Raupach M and Morales Cruz C. Textile-reinforced concrete: Selected case studies. In: *Textile Fibre Composites in Civil Engineering*: Elsevier, 2016, pp. 275–299.
40. Ehlig D, Schladitz F, Frenzel M, et al. Textilbeton - Ausgeführte Projekte im Überblick. *BETON- STAHLBETONBAU* 2012; 107: 777–785.
41. Kromoser B, Preinstorfer P and Kollegger J. Building lightweight structures with carbon-fiber-reinforced polymer-reinforced ultra-high-performance concrete: Research approach, construction materials, and conceptual design of three building components. *STRUCT CONCRETE* 2019; 20: 730–744.
42. May S, Michler H, Schladitz F, et al. Lightweight ceiling system made of carbon reinforced concrete. *STRUCT CONCRETE* 2018; 19: 1862–1872.
43. May S, Steinbock O, Michler H, et al. Precast Slab Structures Made of Carbon Reinforced Concrete. *Structures* 2019; 18: 20–27.
44. Tomoscheit S, Gries T, Horstmann M, et al. Project Life INSUSHELL: Reducing the Carbon Footprint in Concrete Construction. *International Journal of Sustainable Building Technology and Urban Development* 2011; 2: 162–169.
45. Kulas C, Schneider M, Will N, et al. Hinterlüftete Vorhangfassaden aus Textilbeton. *Bautechnik* 2011; 88: 271–280.

46. Shams A, Stark A, Hoogen F, et al. Innovative sandwich structures made of high performance concrete and foamed polyurethane. *COMPOS STRUCT* 2015; 121: 271–279.
47. Řepka J, Vlach T, Laiblová L, et al. Thin Lightweight Panels Made of Textile Reinforced Concrete. *SOL ST PHEN* 2017; 259: 238–243.
48. O'Hegarty R and Kinnane O. Review of precast concrete sandwich panels and their innovations. *CONSTR BUILD MATER* 2020; 233: 117145.
49. Chira A, Kumar A, Vlach T, et al. Textile-reinforced concrete facade panels with rigid foam core prisms. *J SANDW STRUCT MATER* 2016; 18: 200–214.
50. Flansbjerg M, Williams Portal N, Vennetti D, et al. Composite Behaviour of Textile Reinforced Reactive Powder Concrete Sandwich Façade Elements. *INT J CONCR STRUCT M* 2018; 12.
51. Koch A. *Multifunktionale Textilbetonsysteme für die Gebäudehülle*. Aachen: Shaker Verlag, 2018.
52. Valeri P, Guaita P, Baur R, et al. Textile reinforced concrete for sustainable structures: Future perspectives and application to a prototype pavilion. *STRUCT CONCRETE* 2020; 21: 2251–2267.
53. Scholzen A, Chudoba R and Hegger J. Dünnwandiges Schalentragwerk aus textilbewehrtem Beton. *BETON- STAHLBETONBAU* 2012; 107: 767–776.
54. Scholzen A, Chudoba R and Hegger J. Thin-walled shell structures made of textile-reinforced concrete. *STRUCT CONCRETE* 2015; 16: 106–114.
55. Scholzen A, Chudoba R, Hegger J, et al. Leichte Dachschaalen aus Carbonbeton. *BETON- STAHLBETONBAU* 2016; 111: 663–675.
56. Curbach M and Scheerer S. Carbon im Brueckenbau. In: Curbach M (ed.) *24. Dresdner Brückenbausymposium*, 2014, pp. 15–28.
57. Curbach M, Graf W, Jesse D, et al. Segmentbrücke aus textilbewehrtem Beton: Konstruktion, Fertigung, numerische Berechnung. *BETON- STAHLBETONBAU* 2007; 102: 342–352.
58. Bielak J, Will N and Hegger J. Zwei Praxisbeispiele zur Querkrafttragfähigkeit von Brückenplatten aus Textilbeton. *Bautechnik* 2020; 97: 499–507.
59. Helbig T, Unterer K, Kulas C, et al. Fuß- und Radwegbrücke aus Carbonbeton in Albstadt-Ebingen. *BETON- STAHLBETONBAU* 2016; 111: 676–685.
60. Rempel S, Kulas C, Will N, et al. Extremely Light and Slender Precast Pedestrian-Bridge Made Out of Textile-Reinforced Concrete (TRC). In: Hordijk DA and Luković M (eds) *High Tech Concrete: Where Technology and Engineering Meet*. Cham: Springer International Publishing, 2018, pp. 2530–2537.
61. Sydow A, Kurath J and Steiner P. Extrem leichte Brücke aus vorgespanntem Carbonbeton. *BETON- STAHLBETONBAU* 2019; 114: 869–876.
62. C<sup>3</sup> - Carbon Concrete Composite. CUBE, <https://www.bauen-neu-denken.de/cube/> (2021, accessed 1 December 2021).
63. Stelzmann M, Kupke M and Kahnt A. Bauphysikalische Voruntersuchungen in der Planungsphase des CUBE. *BETON- STAHLBETONBAU* 2022.
64. Kupke M. CUBE Projektvorstellung. *Beton- und Stahlbetonbau* 2022.
65. Tietze M, Kirmse S, Kahnt A, et al. The ecological and economic advantages of carbon reinforced concrete - using the C3 result house CUBE especially the BOX value chain as an example. *Civil Engineering Design* 2022.
66. Popescu M. *KnitCrete - Stay-in-place knitted fabric formwork for complex concrete structures*. Dissertation, ETH Zurich, Department of Architecture, 2019.
67. von Zuben M and Cherif C. Robot based Technology for the Production novel Resource-Saving and Cost-Efficient Textile Reinforcement Structures for Direct further Proceedings into Prefabricated Parts. In: *19th World Textile Conference on Textiles at the Crossroads*. (ed AUTEX2019), Ghent, 11-15 June 2019.
68. Schumann A, May M, Schladitz F, et al. Carbonstäbe im Bauwesen. *BETON- STAHLBETONBAU* 2020; 115: 962–971.

69. Cherif C (ed). *Textile Materials for Lightweight Constructions: Technologies - Methods - Materials - Properties*. Berlin/ Heidelberg/ New York/ Dordrecht/ London: Springer-Verlag, 2016.
70. Gries T, Raina M, Quadflieg T, et al. Manufacturing of textiles for civil engineering applications. In: Triantafillou T (ed.) *Textile fibre composites in civil engineering*: Elsevier, 2016, pp. 3–24.
71. Michel A, Zernsdorf K and Mechtcherine V. Mineral-bonded carbon fiber reinforcement for novel concrete construction technologies. In: *Proceedings: International Textile Conference 2019: ADDITC 2019*. (ed Institute für Textilmaschinen und Textile Hochleistungswerkstofftechnik), Dresden, 28.-29.11.2019, p. 84. Dresden.
72. Gries T, Veit D and Wulfhorst B. *Textile technology: An introduction*. 2. ed. Munich: Carl Hanser Fachbuchverlag, 2015.
73. Friese D. *Biologically Inspired Load Adapted 3D-Textile Reinforcement Structures*. Guimaraes (Portugal), 2021.
74. Sankaran V. *Development of a novel multiaxial warp knitting based technology for production of 3D near net shape preforms*. Dissertation, Technische Universität Dresden. Dresden, 2016.
75. Offermann P, Engler T, Gries T, et al. Technische Textilien zur Bewehrung von Betonbauteilen. *BETON- STAHLBETONBAU* 2004; 99: 437–443.
76. Brameshuber W (ed). *Textile reinforced concrete: State-of-the-art-report*. Bagnaux: RILEM Publ, 2006.
77. Kulas C. solidian REBAR D8-CCE (TDS): TDS - Download, <https://solidian.com/de/downloads-de/> (2021, accessed 3 December 2021).
78. Butler M, Mechtcherine V and Hempel S. Experimental investigations on the durability of fibre–matrix interfaces in textile-reinforced concrete. *CEMENT CONCRETE COMP* 2009; 31: 221–231.
79. Carozzi FG and Poggi C. Mechanical properties and debonding strength of Fabric Reinforced Cementitious Matrix (FRCM) systems for masonry strengthening. *COMPOS PART B-ENG* 2015; 70: 215–230.
80. Mader E, Plonka R, Schiek M, et al. Coatings on Alkali-Resistant Glass Fibres for the Improvement of Concrete. *J IND TEXT* 2004; 33: 191–207.
81. Orłowsky J. Durability modelling of glass fibre reinforcement in cementitious environment. *MATER STRUCT* 2005; 38: 155–162.
82. Bobeth W and Berger W (eds). *Textile Faserstoffe: Beschaffenheit und Eigenschaften*. Berlin: Springer, 1993.
83. Ehrenstein GW. *Faserverbund-Kunststoffe: Werkstoffe - Verarbeitung - Eigenschaften*. 2., völlig überarbeitete Auflage. München, Wien: Hanser, 2006.
84. Suter Kunststoff AG. Fasern und Gewebe - Basalt, <https://www.swiss-composite.ch/pdf/I-Basalt-Fasern-Gewebe.pdf> (2011, accessed 3 December 2021).
85. Jäger H, Cherif C, Kirsten M, et al. Influence of processing parameters on the properties of carbon fibres - an overview. *MATERIALWISS WERKST* 2016; 47: 1044–1057.
86. Kimm MK. *Ressourceneffizientes und recyclinggerechtes Design von Faserverbundwerkstoffen im Bauwesen*. Dissertation.
87. Schmiemann A. *Kennwertveränderungen von GFK durch korrosive Einflüsse*. Kassel, 1989.
88. Jongvivatsakul P, Thi CN and Tanapornraweekit G. Mechanical properties of aramid fiber-reinforced composites and performance on repairing concrete beams damaged by corrosion. *J SCI TECHNOL* 2020: 637–644, [https://www.researchgate.net/publication/341388115\\_Mechanical\\_properties\\_of\\_aramid\\_fiber-reinforced\\_composites\\_and\\_performance\\_on\\_repairing\\_concrete\\_beams\\_damaged\\_by\\_corrosion](https://www.researchgate.net/publication/341388115_Mechanical_properties_of_aramid_fiber-reinforced_composites_and_performance_on_repairing_concrete_beams_damaged_by_corrosion) (2020, accessed 3 December 2021).
89. Nguyen CT, Jongvivatsakul P and Tanapornraweekit G. Mechanical Properties of Aramid Fiber Reinforced Concrete. In: *Proceedings of The 21th National Convention on Civil Engineering*, 2016.

90. Elsanadedy HM, Almusallam TH, Alsayed SH, et al. Flexural strengthening of RC beams using textile reinforced mortar – Experimental and numerical study. *COMPOS STRUCT* 2013; 97: 40–55.
91. Larrinaga P, Chastre C, Biscaia HC, et al. Experimental and numerical modeling of basalt textile reinforced mortar behavior under uniaxial tensile stress. *MATER DESIGN* 2014; 55: 66–74.
92. Rambo DAS, Andrade Silva F de, Toledo Filho RD, et al. Effect of elevated temperatures on the mechanical behavior of basalt textile reinforced refractory concrete. *MATER DESIGN* 2015; 65: 24–33.
93. Du Y, Zhang M, Zhou F, et al. Experimental study on basalt textile reinforced concrete under uniaxial tensile loading. *CONSTR BUILD MATER* 2017; 138: 88–100.
94. Li B, Xiong H, Jiang J, et al. Tensile behavior of basalt textile grid reinforced Engineering Cementitious Composite. *COMPOS PART B-ENG* 2019; 156: 185–200.
95. Saravanan D. Spinning the Rocks - Basalt Fibres. *Journal of the Institution of Engineers (India), Part TX: Textile Engineering Division* 2006: 39–45.
96. Shamseldeen A, Elgabbas F and Elshafie H. Tensile behavior of basalt textile-reinforced mortar (BTRM). *Ain Shams Engineering Journal* 2021.
97. Branston J, Das S and Kenno SY. *Mechanical behaviour of basalt fibre reinforced concrete*: Elsevier Ltd, 2016.
98. Jiří Militký, Vladimír Kovačič and Jitka Rubnerová. Influence of thermal treatment on tensile failure of basalt fibers. *ENG FRACT MECH* 2002; 69: 1025–1033.
99. Heins K, Kimm M, Olbrueck L, et al. Long-Term Bonding and Tensile Strengths of Carbon Textile Reinforced Mortar. *MATERIALS* 2020; 13.
100. Donnini J, Corinaldesi V and Nanni A. Mechanical properties of FRCM using carbon fabrics with different coating treatments. *COMPOS PART B-ENG* 2016; 88: 220–228.
101. Wulfhorst B, Gries T and Veit D. *Textile Fertigungsverfahren: Eine Einführung. 2., überarbeitete und erweiterte Auflage. 2., überarb. u. erw. Aufl.* [Place of publication not identified]: CARL HANSER Verlag GMBH &, 2014.
102. Wulfhorst B. *Textile Fertigungsverfahren: Eine Einführung*. München: Hanser, 1998.
103. Mobasher B, Dey V, Cohen Z, et al. Correlation of constitutive response of hybrid textile reinforced concrete from tensile and flexural tests. *CEMENT CONCRETE COMP* 2014; 53: 148–161, <https://www.sciencedirect.com/science/article/pii/S0958946514000948> (2014, accessed 3 December 2021).
104. Peled A, Cohen Z, Pasder Y, et al. Influences of textile characteristics on the tensile properties of warp knitted cement based composites. *CEMENT CONCRETE COMP* 2008; 30: 174–183, <https://www.sciencedirect.com/science/article/pii/S0958946507001503> (2008, accessed 3 December 2021).
105. Mobasher B, Dey V, Bauchmoyer J, et al. Reinforcing Efficiency of Micro and Macro Continuous Polypropylene Fibers in Cementitious Composites. *APPL SCI* 2019; 9: 2189.
106. Wu H-C and Li VC. Fiber/cement interface tailoring with plasma treatment. *CEMENT CONCRETE COMP* 1999; 21: 205–212.
107. Li VC, Wu H-C and Chan Y-W. Effect of Plasma Treatment of Polyethylene Fibers on Interface and Cementitious Composite Properties. *J AM CERAM SOC* 1996; 79: 700–704.
108. Hughes DC. Stress transfer between fibrillated polyalkene films and cement matrices. *Composites* 1984; 15: 153–158.
109. Kobayashi K and Cho R. Flexural Behaviour of Polyethylene Fibre Reinforced Concrete. *International Journal of Cement Composites and Lightweight Concrete* 1981; 1981: 19–25, <https://www.worldcat.org/title/international-journal-of-cement-composites-and-lightweight-concrete/oclc/7939815> (1981, accessed 3 December 2021).
110. Mukhopadhyay S and Khatana S. A review on the use of fibers in reinforced cementitious concrete. *J IND TEXT* 2015; 45: 239–264.

111. Curosu I. *Influence of fiber type and matrix composition on the tensile behavior of strain-hardening cement-based composites (SHCC) under impact loading.: Zum Einfluss der Faserart und Matrixzusammensetzung auf das Zugverhalten von hochduktilen Beton bei Impaktbeanspruchung.* Dissertation. Dresden: TUDpress, 2017.
112. Behbahani H and Nematollahi B. Steel Fiber Reinforced Concrete: A Review. In: *Proceedings of the International Conference on Structural Engineering Construction and Management (ICSECM2011).*
113. Boobalan SC, Karthik RS and Sandeep R. Experimental Investigation of Fibre Reinforced Concrete using Hemp Fibre and Silica Fume. *International Journal of Research in Engineering and Technology* 2017; 06: 112–115.
114. Fernandez J. Flax fiber reinforced concrete - a natural fiber biocomposite for sustainable building materials. In: Brebbia CA and Wilde WP de (eds) *High performance structures and composites: First International Conference on High Performance Structures and Composites, 2002.* Southampton: WIT Press, 2002.
115. Ferrera G, Pepe M, Martinelli E, et al. Influence of Fibres Impregnation on the Tensile Response of Flax Textile Reinforced Mortar Composite Systems. In: Serna P, Llano-Torre A, Marti Vargas JR, et al. (eds) *Fibre Reinforced Concrete: Improvements and Innovations: RILEM-fib International Symposium on FRC (BEFIB) in 2020.* 1st edition. Cham: Springer, 2020.
116. Assaedi H, Shaikh F and Low IM. Characterizations of flax fabric reinforced nanoclay-geopolymer composites. *COMPOS PART B-ENG* 2016; 95: 412–422, <https://www.sciencedirect.com/science/article/abs/pii/S1359836816302244> (2016, accessed 3 December 2021).
117. Sen T and Jagannatha Reddy HN. Strengthening of RC beams in flexure using natural jute fibre textile reinforced composite system and its comparative study with CFRP and GFRP strengthening systems. *International Journal of Sustainable Built Environment* 2013; 2: 41–55.
118. Fidelis MEA, Toledo Filho RD, Andrade Silva F de, et al. Interface characteristics of jute fiber systems in a cementitious matrix. *CEMENT CONCRETE RES* 2019; 116: 252–265.
119. R. Figueiro, C. Pereira, S. Jalali, et al. The mechanical properties of braided reinforced composites for application in concrete structures. *MATER SCI+* 2006.
120. Yan L, Kasal B and Huang L. A review of recent research on the use of cellulosic fibres, their fibre fabric reinforced cementitious, geo-polymer and polymer composites in civil engineering. *COMPOS PART B-ENG* 2016; 92: 94–132.
121. C. Asasutjarit, J. Hirunlabh, J. Khedari, et al. Development of coconut coir-based lightweight cement board. *CONSTR BUILD MATER* 2007; 21: 277–288, <https://www.sciencedirect.com/science/article/pii/S0950061805002643> (2007, accessed 3 December 2021).
122. Baruah P and Talukdar S. A comparative study of compressive, flexural, tensile and shear strength of concrete with fibres of different origins. *Indian concrete journal* 2007; 81: 17–24.
123. Singh SM. Alkali resistance of some vegetable fibers and their adhesion with Portland-cement. *RES IND* 1985; 30: 121–126.
124. Büttner T, Orłowsky J and Raupach M. Erhöhung der Dauerhaftigkeit textiler Beton-Bewehrungen durch Epoxidharztränkung. *Bautechnik* 2011; 88: 263–270.
125. Hahn L. *Entwicklung einer In-situ-Beschichtungs- und Trocknungstechnologie für multiaxiale Gelegestrukturen mit hohem Leistungsvermögen.* Dissertation. Dresden: TUDpress, 2020.
126. Quadflieg T, Leimbrink S, Gries T, et al. Effect of coating type on the mechanical performance of warp-knitted fabrics and cement-based composites. *J COMPOS MATER* 2018; 52: 2563–2576.
127. Lorenz E. *Endverankerung und Übergreifung textiler Bewehrungen in Betonmatrices: End Anchorage and Overlapping of Textile Reinforcements in Concrete.* Dissertation, Technische Universität Dresden. Dresden.

128. Raooof SM, Koutas LN and Bournas DA. Bond between textile-reinforced mortar (TRM) and concrete substrates: Experimental investigation. *COMPOS PART B-ENG* 2016; 98: 350–361.
129. Kulas C (ed). *Zum Tragverhalten getränkter textiler Bewehrungselemente für Betonbauteile*. Zugl.: Aachen, Techn. Hochsch., Diss., 2013. 1. Aufl. Aachen: IMB, 2013.
130. Sika Deutschland GmbH. Biresin CR84 (Compositeharz-System): Technical datasheet, [www.sika.de](http://www.sika.de) (2016, accessed 10 August 2021).
131. Bacuplast Faserverbundtechnik GmbH. Technical datasheet: Epoxid-Laminierharz-System EP 211/EPH 411, <https://www.bacuplast.de/EP211+411.pdf> (2018, accessed 10 August 2021).
132. CHT Germany GmbH. TECOSIT R H-0N: Technical datasheet (2019, accessed 3 December 2021).
133. Lefatex Chemie GmbH. Specification sheet - Lefasol VL 90/1 (2014, accessed 7 July 2021).
134. Lefatex Chemie GmbH. Specification sheet - Lefasol BT 91001-1 (2017, accessed 3 December 2021).
135. Dyckerhoff GmbH. Technical Data Sheet.: Dyckerhoff MIKRODUR ...vom Feinsten., <https://www.dyckerhoff.com/documents/209745/971601/Dyckerhoff+MIKRODUR...+vom+Feinsten.pdf/fec58a06-bb60-7c5f-2022-b79a251b8922> (2016, accessed 15 July 2021).
136. Mechtcherine V, Michel A, Liebscher M, et al. Mineral-impregnated carbon fiber composites as novel reinforcement for concrete construction: Material and automation perspectives. *AUTOMAT CONSTR* 2020; 110: 103002.
137. Nativ R, Peled A, Mechtcherine V, et al. Micro- and nanoparticle mineral coating for enhanced properties of carbon multifilament yarn cement-based composites. *COMPOS PART B-ENG* 2017; 111: 179–189.
138. Schneider K, Lieboldt M, Liebscher M, et al. Mineral-Based Coating of Plasma-Treated Carbon Fibre Rovings for Carbon Concrete Composites with Enhanced Mechanical Performance. *MATERIALS* 2017; 10.
139. Sika Deutschland GmbH. Biresin CR201 Harz: Technical datasheet. Compositeharz-System für Heisshärtung, [www.sika.de](http://www.sika.de) (accessed 10 August 2021).
140. Sika Deutschland GmbH. Epolam 2092 Epoxidharz: Technical datasheet. EPOXID-LAMINIERHARZ. Hochtemperatur Tg 225 °C, [www.sika.de](http://www.sika.de) (2016, accessed 10 August 2021).
141. Kruppke I. *Entwicklung von Methoden zur Realisierung von maßgeschneiderten Adhäsionseigenschaften von faserbasierten Hochleistungswerkstoffen für Composites*. Dissertation. Dresden: TUDpress, 2018.
142. Schneider K, Michel A, Liebscher M, et al. Verbundverhalten mineralisch gebundener und polymergebundener Bewehrungsstrukturen aus Carbonfasern bei Temperaturen bis 500 °C. *BETON- STAHLBETONBAU* 2018; 113.
143. Schneider K, Michel A, Liebscher M, et al. Mineral-impregnated carbon fibre reinforcement for high temperature resistance of thin-walled concrete structures. *CEMENT CONCRETE COMP* 2018; 97.
144. Silva FdA, Butler M, Hempel S, et al. Effects of elevated temperatures on the interface properties of carbon textile-reinforced concrete. *CEMENT CONCRETE COMP* 2014; 48: 26–34.
145. Kruppke I, Butler M, Schneider K, et al. Carbon Fibre Reinforced Concrete: Dependency of Bond Strength on T<sub>g</sub> of Yarn Impregnating Polymer. *Materials Sciences and Applications* 2019; 10: 328–348.
146. Mechtcherine V, Schneider K and Brameshuber W. Mineral-based matrices for textile-reinforced concrete. In: *Textile Fibre Composites in Civil Engineering*: Elsevier, 2016, pp. 25–43.
147. Neef T and Müller S. Neue Carbonfaserbewehrung für Beton-3D-Druck und andere digitale Betonbauverfahren. In: *12. Carbon- und Textilbetontage 2020: Proceedings*. (ed TUDALIT e. V., C<sup>3</sup> - Carbon Concrete Composite e.V., Schön K and Schladitz F), Dresden, 22.-23.09.2020. Dresden.

148. Hengstermann M, Schneider K and Scheffler C. Zwanzig20 - Carbon Concrete Composites C<sup>3</sup> - V 2.4-III: Entwicklung von Commingling-Garnen mit thermoplastischen Binder-Filamenten; Projekt-Schlussbericht Projektlaufzeit: 01.04.2017 bis 31.03.2019, Dresden, 2019.
149. Janetzko S, Kravaev P, Gries T, et al. Textile reinforcement with spread and commingled yarn structures. In: Brameshuber W (ed.) *International RILEM Conference on Material Science // Textile reinforced concrete: 2nd ICTRC, [International Conference of Textile Reinforced Concrete]*. Bagneux: RILEM Publ, 2010, pp. 37–44.
150. Glowania M, Gries T, Schoene J, et al. Innovative Coating Technology for Textile Reinforcements of Concrete Applications. *KEY ENG MAT* 2011; 466: 167–173.
151. Preinstorfer P. *Zur Spaltrissbildung von textilbewehrtem Beton*. Dissertation, TU Wien, 2019.
152. Fédération internationale du béton. *Fib model code for concrete structures 2010*. Lausanne: Ernst & Sohn, 2013.
153. Bentur A and Mindess S. *Fibre reinforced cementitious composites*. Second edition. Boca Raton: CRC Press, 2019.
154. Raupach M. Epoxy-impregnated textiles in concrete – Load bearing capacity and durability. In: *ICTRC'2006 - 1st International RILEM Conference on Textile Reinforced Concrete*, Aachen, Germany, 06.09.2006 - 07.09.2006, pp. 77–88: RILEM Publications SARL.
155. Schumann A, May M and Curbach M. Carbonstäbe im Bauwesen. *BETON- STAHLBETONBAU* 2018; 113: 868–876.
156. Victor C. Li, Cynthia Wu, Shuxin Wang, Atsuhisa Ogawa, and Tadashi Saito. Interface Tailoring for Strain-Hardening Polyvinyl Alcohol-Engineered Cementitious Composite (PVA-ECC). *ACI Materials Journal*; 99.
157. Lorenz E. *Endverankerung und Übergreifung textiler Bewehrungen in Betonmatrices: Schriftenreihe Konstruktiver Ingenieurbau Dresden ; 39*. Dresden: Inst. für Massivbau, Techn. Univ, 2015.
158. Bielak J, Spelter A, Will N, et al. Verankerungsverhalten textiler Bewehrungen in dünnen Betonbauteilen. *Beton- und Stahlbetonbau* 2018; 113: 515–524.
159. Cherif C. *Textile Werkstoffe für den Leichtbau: Techniken - Verfahren - Materialien - Eigenschaften*. Berlin, Heidelberg: Springer, 2011.
160. Richter M and Zastrau BW. On the nonlinear elastic properties of textile reinforced concrete under tensile loading including damage and cracking. *Materials Science and Engineering: A* 2006; 422: 278–284.
161. Zastrau B, Richter M and Lepenies I. On the Analytical Solution of Pullout Phenomena in Textile Reinforced Concrete. *Journal of Engineering Materials and Technology* 2003; 125: 38–43.
162. Banholzer B. *Bond behaviour of a multi-filament yarn embedded in a cementitious matrix*. Zugl.: Aachen, Techn. Hochsch., Diss., 2004. 1. Aufl. Aachen: Mainz, 2004.
163. Brameshuber W, Banholzer B and Brümmer G. Ansatz für eine vereinfachte Auswertung von Faser Ausziehversuchen. *Beton- und Stahlbetonbau* 2000; 95: 702–706.
164. Lorenz E and Ortlepp R. Bond Behavior of Textile Reinforcements - Development of a Pull-Out Test and Modeling of the Respective Bond versus Slip Relation. In: Parra-Montesinos GJ (ed.) *High Performance Fiber Reinforced Cement Composites 6: Hprfcc 6*. Dordrecht: Springer Netherlands, 2012, pp. 479–486.
165. Hartig J, Häußler-Combe U and Schicktanz K. Influence of bond properties on the tensile behaviour of Textile Reinforced Concrete. *Cement and Concrete Composites* 2008; 30: 898–906.
166. Wendler J, Hahn L, Farwig K, et al. Entwicklung eines neuartigen Prüfverfahrens zur Untersuchung der Zugfestigkeit von Fasersträngen für textile Bewehrungsstrukturen: Analysis of the tensile mechanical characteristics of flexible carbon fibre strands and development of a novel test method. *BAUINGENIEUR-GERMANY* 2020; 95: 325–334.



167. Valeri P, Fernández Ruiz M and Muttoni A. Tensile response of textile reinforced concrete. *CONSTR BUILD MATER* 2020; 258: 119517.
168. Deutsches Institut für Bautechnik Z-31.10-182. National technical approval (abZ)/ General construction technique permit (aBG); Allgemeine bauaufsichtliche Zulassung/ Allgemeine Bauartgenehmigung (abZ/aBG).
169. Schumann A. *Experimentelle Untersuchungen des Verbundverhaltens von Carbonstäben in Betonmatrices*. Dissertation, Technische Universität Dresden. Dresden, 2020.
170. Nanni A, Luca A de and Jawaheri Zadeh H. *Reinforced concrete with FRP bars: Mechanics and design*. Boca Raton, FL: CRC Press, 2014.
171. Mufti AA and Neale KW. State-of-the-art of FRP and SHM applications in bridge structures in Canada. *Composite Research Journal* 2010.
172. Enomoto T, Grace NF and Harada T. Life Extension of Prestressed Concrete Bridges Using CFCC Tendons and Reinforcements. In: CICE (ed.) *Proceedings of 6th International Conference on FRP Composites in Civil Engineering (CICE)*. Rome, 2012.
173. Grace NF, Navarre FC, Nacey RB, et al. Design-Construction of Bridge Street Bridge — First CFRP Bridge in the United States. *PCI J* 2002; 47: 20–35,  
[https://www.pci.org/PCI/Publications/PCI\\_Journal/Issues/2002/September-October/Design-Construction\\_of\\_Bridge\\_Street\\_Bridge\\_-\\_First\\_CFRP\\_Bridge\\_in\\_the\\_United\\_States.aspx](https://www.pci.org/PCI/Publications/PCI_Journal/Issues/2002/September-October/Design-Construction_of_Bridge_Street_Bridge_-_First_CFRP_Bridge_in_the_United_States.aspx) (2002, accessed 3 December 2021).
174. Flemming M, Ziegmann G and Roth S. *Faserverbundbauweisen*. Berlin, Heidelberg: Springer Berlin Heidelberg, 1995.
175. Böhm R, Thieme M, Wohlfahrt D, et al. Reinforcement Systems for Carbon Concrete Composites Based on Low-Cost Carbon Fibers. *Fibers* 2018; 6: 56.
176. R. Figueiro, C. Pereira, S. Jalali, et al. The mechanical properties of braided reinforced composites for application in concrete structures. *MATER SCI+* 2006,  
[https://core.ac.uk/display/55606889?utm\\_source=pdf&utm\\_medium=banner&utm\\_campaign=pdf-decoration-v1](https://core.ac.uk/display/55606889?utm_source=pdf&utm_medium=banner&utm_campaign=pdf-decoration-v1) (2006, accessed 3 December 2021).
177. Cherif C and Hahn L. Fortschritte bei Fertigung von profilierten Carbonpolymergarnen mit höchsten Verbundeigenschaften. *TUDALIT-Magazin* 2020.
178. Scheurer M, Quenzel P, Nölke P, et al. Investigating the feasibility of using carbon fibre tapes as reinforcement for 3D concrete printing. *J CIVIL ENG DES* 2021.
179. Peled A and Bentur A. Geometrical characteristics and efficiency of textile fabrics for reinforcing cement composites. *CEMENT CONCRETE RES* 2000; 30: 781–790.
180. Adam R, Schneider K, Wohlfahrt D, et al. Zwanzig20 - Carbon Concrete Composites C<sup>3</sup> - V 1.1: Herstell- und Verarbeitungsprozesse von Carbonbeton: TP 10: Entwicklung von Herstell- und Verarbeitungsprozessen von Carbonbeton. Projekt-Schlussbericht; Projektlaufzeit: 01.12.2015 bis 31.03.2018, Dresden, 2018.
181. Janetzko S. *Methodik zur Gestaltung von Bewehrungssystemen für textildbewehrten Beton*. Dissertation, Technische Hochschule Aachen. Aachen, 2013.
182. Hausding J, Lorenz E, Ortlepp R, et al. Application of stitch-bonded multi-ply made by using the extended warp knitting process: Reinforcements with symmetrical layer arrangement for concrete. *TJTI* 2011; 102: 726–738.
183. Dolatabadi MK, Janetzko S and Gries T. Geometrical and mechanical properties of a non-crimp fabric applicable for textile reinforced concrete. *TJTI* 2014; 105: 711–716.
184. Perry G, Dittel G, Gries T, et al. Mutual Effect of Textile Binding and Coating on the Structural Performance of TRC Beams. *J MATER CIVIL ENG* 2020; 32: 4020232.
185. Stolyarov O, Quadflieg T and Gries T. Effects of fabric structures on the tensile properties of warp-knitted fabrics used as concrete reinforcements. *TEXT RES J* 2015; 85: 1934–1945.

186. Roye A. *Hochleistungsdoppelraschelprozess für Textilbetonanwendungen*. Dissertation, Technische Hochschule Aachen. Aachen, 2007.
187. Quadflieg T, Stolyarov O and Gries T. Influence of the fabric construction parameters and roving type on the tensile property retention of high-performance rovings in warp-knitted reinforced fabrics and cement-based composites. *J IND TEXT* 2017; 47: 453–471.
188. Köckritz U. *In-Situ Polymerbeschichtungen zur Strukturstabilisierung offener nähgewirkter Gelege: In-situ polymer coating for the structural stabilisation of open grid warp knitted fabrics*. Dissertation, Technische Universität Dresden. Dresden, 2007.
189. Koeckritz U, Cherif C, Weiland S, et al. In-Situ Polymer Coating of Open Grid Warp Knitted Fabrics for Textile Reinforced Concrete Application. *J IND TEXT* 2010; 40: 157–169.
190. Hahn L, Rittner S, Nuss D, et al. Development of Methods to Improve the Mechanical Performance of Coated Grid-Like Non-Crimp Fabrics for Construction Applications. *FIBRES TEXT EAST EUR* 2019; 27: 51–58.
191. Pidun K. *Ansatz zur Formgebung von Textilbeton im frischen Zustand*. Dissertation, Rheinisch-Westfälische Technische Hochschule Aachen. Aachen, 2019.
192. Dittel G, Quadflieg T, Koch A, et al. Tailored warp knitted reinforced textiles for construction applications. In: *The Fiber Society 2017 Spring Conference Next Generation Fibers for Smart Products*. (ed The Fiber Society), Aachen, 17.-19.05.
193. Quadflieg TA. *Gewirkte Verstärkungstextilien mit kohlenstofffaserbasierter Sensorik im Verbundwerkstoff mit mineralischer Matrix*. Dissertation, Shaker Verlag GmbH; RWTH Aachen.
194. Quadflieg T, Stolyarov O and Gries T. Carbonfaserbewehrung als Sensor für Bauwerke. *BETON- STAHLBETONBAU* 2017; 112: 541–544.
195. Quadflieg T, Stolyarov O and Gries T. Carbon rovings as strain sensors for structural health monitoring of engineering materials and structures. *J STRAIN ANAL ENG* 2016; 51: 482–492.
196. Goldfeld Y, Quadflieg T, Ben-Aarosh S, et al. Micro and macro crack sensing in TRC beam under cyclic loading. *J MECH MATER STRUCT* 2017; 12: 579–601.
197. Goldfeld Y, Quadflieg T and Gries T. Sensing capabilities of carbon based TRC beam from slack to pull-out mechanism. *COMPOS STRUCT* 2017; 181: 294–305, <https://www.sciencedirect.com/science/article/pii/S0263822316322309> (2017, accessed 1 December 2021).
198. Goldfeld Y, Rabinovitch O, Fishbain B, et al. Sensory carbon fiber based textile-reinforced concrete for smart structures. *J INTEL MAT SYST STR* 2016; 27: 469–489.
199. Quadflieg T, Goldfeld Y, Dittel G, et al. New Age Advanced Smart Water Pipe Systems Using Textile Reinforced Concrete. *Procedia Manufacturing* 2018; 21: 376–383.
200. Rittner S, Speck K, Seidel A, et al. Development of Loop-Shaped Textile Anchoring Reinforcements Based on Multiaxial Warp Knitting Technology. *FIBRES TEXT EAST EUR*, 2020, pp. 64–71.
201. Hahn L, Rittner S, Bauer C, et al. Development of alternative bondings for the production of stitch-free non-crimp fabrics made of multiple carbon fiber heavy tows for construction industry. *J IND TEXT* 2018; 48: 660–681.
202. Hegger J, Schneider HN, Kulas C, et al. Dünnwandige, großformatige Fassadenelemente aus Textilbeton. In: *4th Colloquium on Textile Reinforcement Structures (CTRS4)*, pp. 541–552.
203. Hegger J, Kulas C and Horstmann M. Spatial Textile Reinforcement Structures for Ventilated and Sandwich Facade Elements. *Advances in Structural Engineering* 2012; 15: 665–675.
204. Hahn L, Rittner S and Cherif C. Fertigungstechnologie zur Herstellung von vorgeformten textilen Bewehrungen. In: *10. Carbon- und Textilbetontage: Proceedings*. (ed TUDALIT e. V. and C<sup>3</sup> - Carbon Concrete Composite e.V.), Dresden, 25.-26.09.2018. Dresden.

205. Hahn L, Rittner S and Cherif C. Highly Automated Production of Preformed Textile Reinforcements for a Variety of Construction Applications.: Vortrag. In: *4th International Composites Congress 2018*.
206. Hahn L. V1.1 - Innovative Fertigungstechnologie zur Herstellung von vorgeformten textilen Bewehrungen. In: *10. Carbon- und Textilbetontage: Proceedings*. (ed TUDALIT e. V. and C<sup>3</sup> - Carbon Concrete Composite e.V.), Dresden, 25.-26.09.2018, pp. 78–79. Dresden.
207. Hahn L. *Prototype of a production technology for highly efficient manufacturing of preformed textile reinforcements for construction applications.: Vortrag/Speaker's Platform*. Barcelona, 2019.
208. Younes A, Seidel A, Rittner S, et al. Innovative textile Bewehrungen für hochbelastbare Betonbauteile. *BETON- STAHLBETONBAU* 2015; 110: 16–21.
209. Rittner S, Steinberg J, Klug P, et al. Inherent evolution - Development of a technique for the production of 3D reinforcing grids, based on multiaxial warp knitting technology. *Technical Textiles Kettenwirk-Praxis* 2018; 52: 28–29.
210. Sankaran V, Younes A, Engler T, et al. A novel processing solution for the production of spatial three-dimensional stitch-bonded fabrics. *TEXT RES J* 2012; 82: 1531–1544.
211. Sankaran V, Rittner S, Hahn L, et al. Development of multiaxial warp knitting technology for production of three-dimensional near net shape shell preforms. *TEXT RES J* 2017; 87: 1226–1241.
212. Gries T, Wulfhorst B and Veit D. *Textile Fertigungsverfahren: Eine Einführung*. 3., überarbeitete und erweiterte Auflage. München: Carl Hanser Verlag GmbH & Co. KG, 2018.
213. Roye A and Gries T. 3-D Textiles for Advanced Cement Based Matrix Reinforcement. *J IND TEXT* 2007; 37: 163–173.
214. Armakan DM and Roye A. A study on the compression behavior of spacer fabrics designed for concrete applications. *FIBER POLYM* 2009; 10: 116–123.
215. Haik R, Adiel Sasi E and Peled A. Influence of three-dimensional (3D) fabric orientation on flexural properties of cement-based composites. *CEMENT CONCRETE COMP* 2017; 80: 1–9.
216. El Kadi M, Tysmans T, Verbruggen S, et al. Experimental study and benchmarking of 3D textile reinforced cement composites. *CEMENT CONCRETE COMP* 2019; 104: 103352.
217. Concrete Canvas Ltd. WAS IST CC?, <https://www.concretecanvas.com/de/concrete-canvas/> (accessed 29 November 2021).
218. Han F, Chen H, Jiang K, et al. Influences of geometric patterns of 3D spacer fabric on tensile behavior of concrete canvas. *CONSTR BUILD MATER* 2014; 65: 620–629.
219. Han F, Chen H, Zhang W, et al. Influence of 3D spacer fabric on drying shrinkage of concrete canvas. *J IND TEXT* 2016; 45: 1457–1476.
220. Li H, Zhang W, Chen H, et al. Lattice modeling for the influence of geometrical patterns of 3D spacer fabric on tensile behavior of concrete canvas. *J SANDW STRUCT MATER* 2021, <https://doi.org/10.1177/10996362211020430> (2021, accessed 2 December 2021).
221. V. Fraas Solutions in Textile GmbH. V. FRAAS Solutions in Textile löst Verbindungsproblem von 3D biaxialen Bewehrungsgittern für Beton. In: TUDALIT e.V. (ed.) *TUDALIT - Magazin: Leichter bauen -Zukunft formen*. Dresden, 2015.
222. International Organisation for Standardization ISO 3572. Textiles - Weaves - Definitions of general terms and basic weaves.
223. Peled A, Bentur A and Yankelevsky D. Woven fabric reinforcement of cement matrix. *ADV CEM BASED MATER* 1994; 1: 216–223.
224. Perez-Pena M and Mobasher B. Mechanical properties of fiber reinforced lightweight concrete composites. *CEMENT CONCRETE RES* 1994; 24: 1121–1132.
225. Weise D, Vorhof M, Brünler R, et al. Reduction of weaving process-induced warp yarn damage and crimp of leno scrims based on coarse high-performance fibers. *TEXT RES J* 2019; 89: 3326–3341.

226. Hausding J, Kleicke R, Döbrich O, et al. Improved Stitch-Bonded and Leno-Woven Multiplies for Composites. In: *SAMPE 2009*, 2009.
227. Weise D. *Konstruktiv-technologische Entwicklung von Hochleistungsdrehergeweben für Hightech-Anwendungen*. Dissertation, Technische Universität Dresden. Dresden, 2020.
228. Kleicke R, Hausding J, Cherif C, et al. Research regarding the use of Stitch-bonded and Leno woven non Crimp Fabrics Reinforcements in Textile Reinforced Concrete. In: Brameshuber W (ed.) *Textile reinforced concrete: 2nd ICTRC, [International Conference of Textile Reinforced Concrete]*. Bagneux: RILEM Publ, 2010, pp. 45–55.
229. Rampini MC, Zani G, Colombo M, et al. Mechanical Behaviour of TRC Composites: Experimental and Analytical Approaches. *APPL SCI* 2019; 9: 1492, <https://www.mdpi.com/2076-3417/9/7/1492> (2019, accessed 1 December 2021).
230. Colombo IG, Magri A, Zani G, et al. Erratum to: Textile Reinforced Concrete: experimental investigation on design parameters. *MATER STRUCT* 2013; 46: 1953–1971.
231. Lenz C, Schröter A and Gries T. Concrete and plaster reinforcement by multiple leno fabrics. In: *2nd International Glass Fiber Symposium, Aachen, Germany, 25 - 30 May 2014*, p. 310.
232. Brennan J, Pedreschi R, Walker P, et al. The potential of advanced textiles for fabric formwork. In: *Proceedings of the Institution of Civil Engineers*, pp. 229–237.
233. Popescu M, Rippmann M, van Mele T, et al. Complex concrete casting: knitting stay-in-place fabric formwork. In: *Proceedings of the International Association for Shell and Spatial Structures (IASS) Symposium 2016*. (ed International Association for Shell and Spatial Structures). Madrid, Spain.
234. Popescu M, Reiter L, Liew A, et al. Building in concrete with a knitted stay-in-place formwork: Prototype of a concrete shell bridge. *Structures* 2018; 14: 322–332, <https://www.sciencedirect.com/science/article/abs/pii/S2352012418300262?via%3Dihub> (2018, accessed 1 December 2021).
235. Popescu M, Rippmann M, Liew A, et al. Concrete shell built using a cable-net and knitted formwork. *DETAIL structure* 2019; 1: 10–11.
236. Popescu M, Rippmann M, Liew A, et al. Structural design, digital fabrication and construction of the cable-net and knitted formwork of the KnitCandela concrete shell. *Structures* 2020.
237. Jonas F, Born L, Möhl C, et al. Towards branched supporting structures out of concrete-FRP composites inspired from natural branchings. In: *Proceedings of the IASS Annual Symposium 2018: Reimagining material and design*. Boston: International Association for Shell and Spatial Structures (IASS), 2018.
238. Feix J. Gestickte Bewehrungen. In: *9. Carbon- und Textilbetontagung: Proceedings*. (ed TUDALIT e.V. and C<sup>3</sup> - Carbon Concrete Composite e.V.), Dresden, 26.-27.09.2017, p. 47. Dresden.
239. Beckmann B, Bielak J, Scheerer S, et al. Standortübergreifende Forschung zu Carbonbetonstrukturen im SFB/TRR 280. *Bautechnik* 2021; 98: 232–242.
240. FibR GmbH and Dörstelmann M. Exhibition Architecture and Mobile Structures, <https://www.fibr.tech/gallery> (2021, accessed 23 November 2021).
241. Knippers J and Jan Knippers Ingenieure. BUGA Faserpavillon: Bundesgartenschau Heilbronn 2019, <https://www.janknippers.com/de/archives/portfolio-type/faserpavillon-bundesgartenschau-heilbronn-2019> (2019, accessed 1 December 2021).
242. Cherif C, Hahn L, Zuben M, et al. Zwanzig20 - Carbon Concrete Composites C<sup>3</sup> - V 4.1: Multiaxiale Garnablage im automatisierten Umlaufprozess (Multi-2D Druck); Teilprojekt V4.1-II: Entwicklung einer neuen Technologie zur direkten Schalungsintegrierten Garnablage für die Herstellung von Textilbeton-Fertigteilen: Schlussbericht; Projektlaufzeit: 01.08.2016 bis 31.10.2019, Dresden, 2019.

243. von Zuben M and Cherif C. Robotergestützte Fertigung von Bewehrungsstrukturen für das Bauen mit Carbonbeton. In: *10. Carbon- und Textilbetontage: Proceedings*. (ed TUDALIT e. V. and C<sup>3</sup> - Carbon Concrete Composite e.V.), Dresden, 25.-26.09.2018, pp. 104–105. Dresden.
244. TUDALIT e. V. and C<sup>3</sup> - Carbon Concrete Composite e.V. (eds). *10. Carbon- und Textilbetontage: Proceedings*. Dresden, 2018.
245. Minsch N, Herrmann FH, Gereke T, et al. Analysis of Filament Winding Processes and Potential Equipment Technologies. *Procedia CIRP* 2017; 66: 125–130.
246. Minsch N, Müller M, Gereke T, et al. Novel fully automated 3D coreless filament winding technology. *J COMPOS MATER* 2018; 52: 3001–3013.
247. Minsch N, Müller M, Gereke T, et al. 3D truss structures with coreless 3D filament winding technology. *J COMPOS MATER* 2018.
248. Minsch N. *Verfahrens- und Methodenentwicklung für die generative Fertigung von komplexen Leicht-baustrukturen in Hybridbauweise: Process- und method development for the generative manufacturing of complex lightweight structures in hybrid design*. Dissertation, Technische Universität Dresden. Dresden, 2018.
249. Mechtcherine V, Michel A, Liebscher M, et al. Neue Carbonfaserbewehrung für digitalen automatisierten Betonbau. *BETON- STAHLBETONBAU* 2019; 114: 947–955.
250. Knippers J, Koslowski V, Solly J, et al. Modular coreless filament winding for lightweight systems in architecture. In: CICE (ed.) *CICE 2016 8th International Conference on Fibre-Reinforced Polymer (FRP) Composites in Civil Engineering*. Hong Kong, 2016.
251. Solly J, Frueh N, Saffarian S, et al. ICD/ITKE Research Pavilion 2016/2017: Integrative Design of a Composite Lattice Cantilever. In: *Conference Proceedings: IASS 2018 Creativity in Structural Design*. Massachusetts, 2018.
252. TUDALIT e.V. and C<sup>3</sup> - Carbon Concrete Composite e.V. (eds). *9. Carbon- und Textilbetontagung: Proceedings*. Dresden, 2017.
253. TUDALIT e. V. and C<sup>3</sup> - Carbon Concrete Composite e.V. (eds). *10. Carbon- und Textilbetontage: Tagungsband*. Dresden, 2018.
254. TUDALIT e. V. and C<sup>3</sup> – Carbon Concrete Composite e. V. (eds). *11. Carbon- und Textilbetontage: Proceedings*. Dresden, 2019.
255. TUDALIT e. V., C<sup>3</sup> - Carbon Concrete Composite e.V., Schön K, et al. (eds). *12. Carbon- und Textilbetontage 2020: Proceedings*. Dresden, 2020.
256. Sonderforschungsbereich - SFB 532: Textilbewehrter Beton - Grundlagen für die Entwicklung einer neuartigen Technologie. Arbeits- und Ergebnisbericht, Lehrstuhl und Institut für Massivbau Aachen, Aachen, 2002.
257. Sonderforschungsbereich 528 - Abschlussbericht: Textile Bewehrungen zur bautechnischen Verstärkung und Instandsetzung, Technische Universität Dresden, Dresden, 2011.