

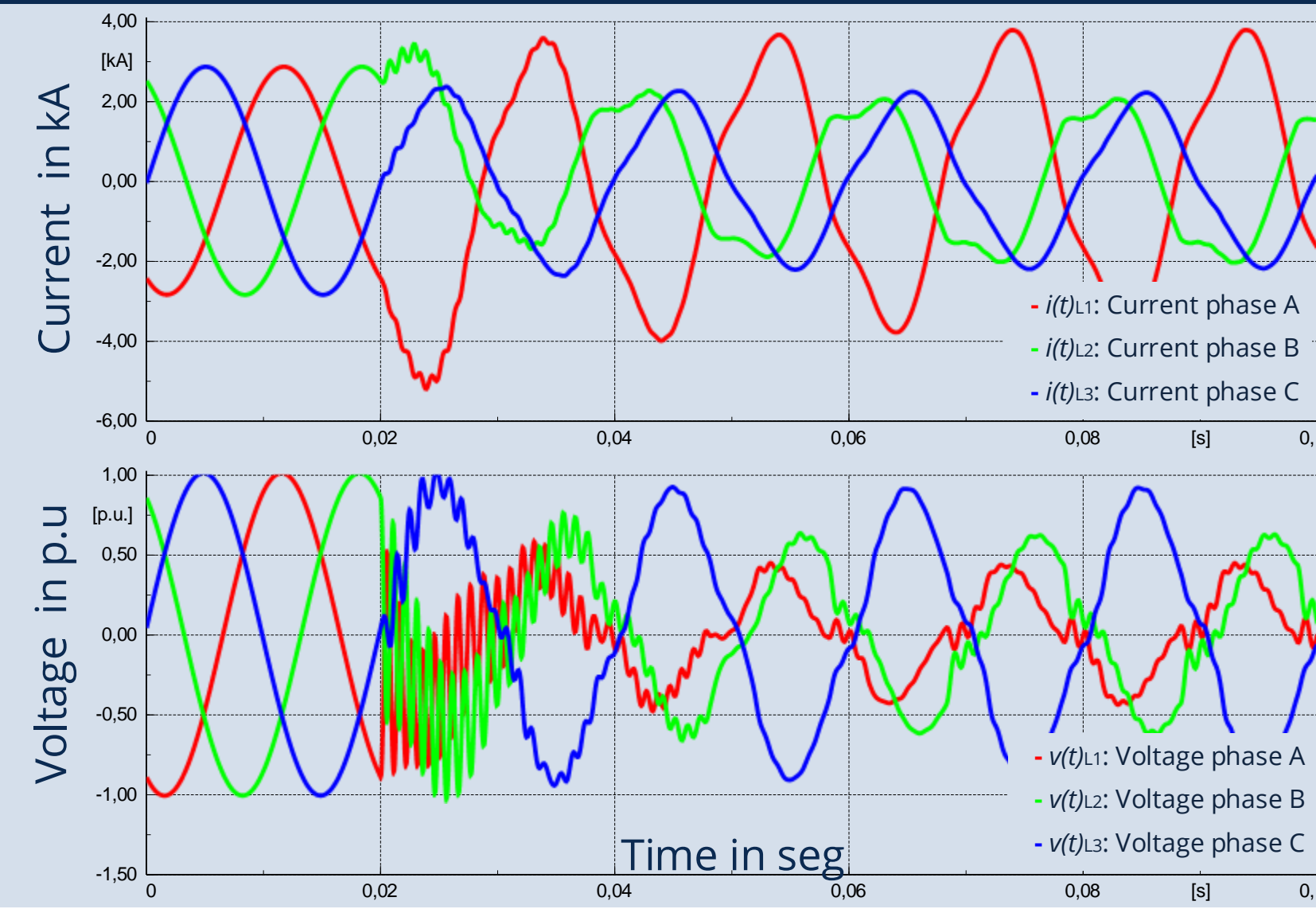
Transmission Lines Protection using Digital Morphologic Filter of Fault-generated High-frequency Transient Signals

Juan Carlos Quispe, Carlo Liebermann, Peter Schegner TU Dresden

Motivation

- The increase of renewable energy sources (RES) involves the dependence of power electronics in electrical networks.
- The RES fault behavior is quite varied as it depends on their structural design features and control system settings.
- Traditional protection devices are experiencing challenges due to the increase of RES.
- Therefore, it is necessary to study new protection algorithms to avoid this effect.
- A new scheme is proposed through the use of fault-generated high-frequency transient signals based on mathematical morphology.

Protection relays challenges

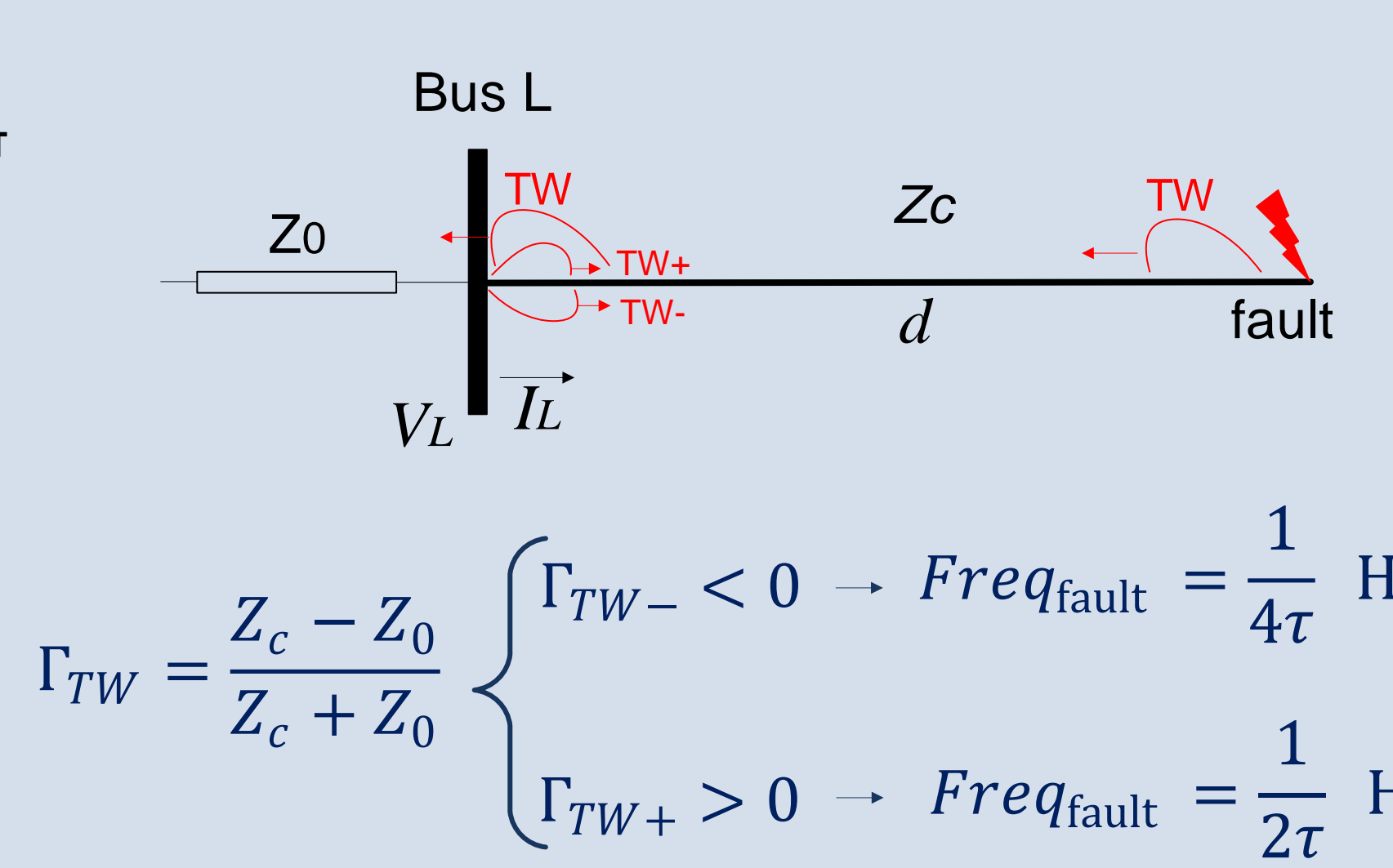
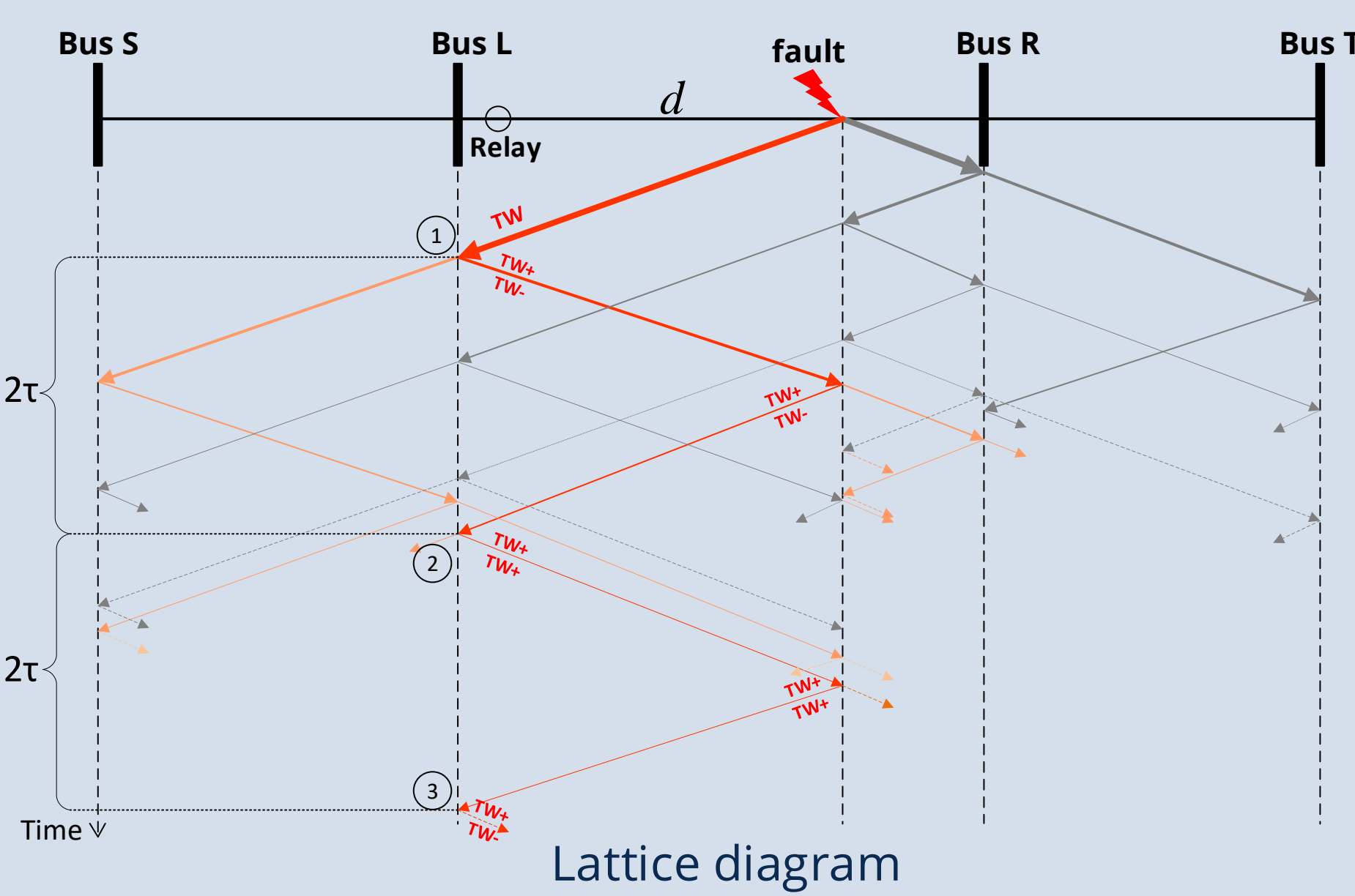


Case: Two-phase fault

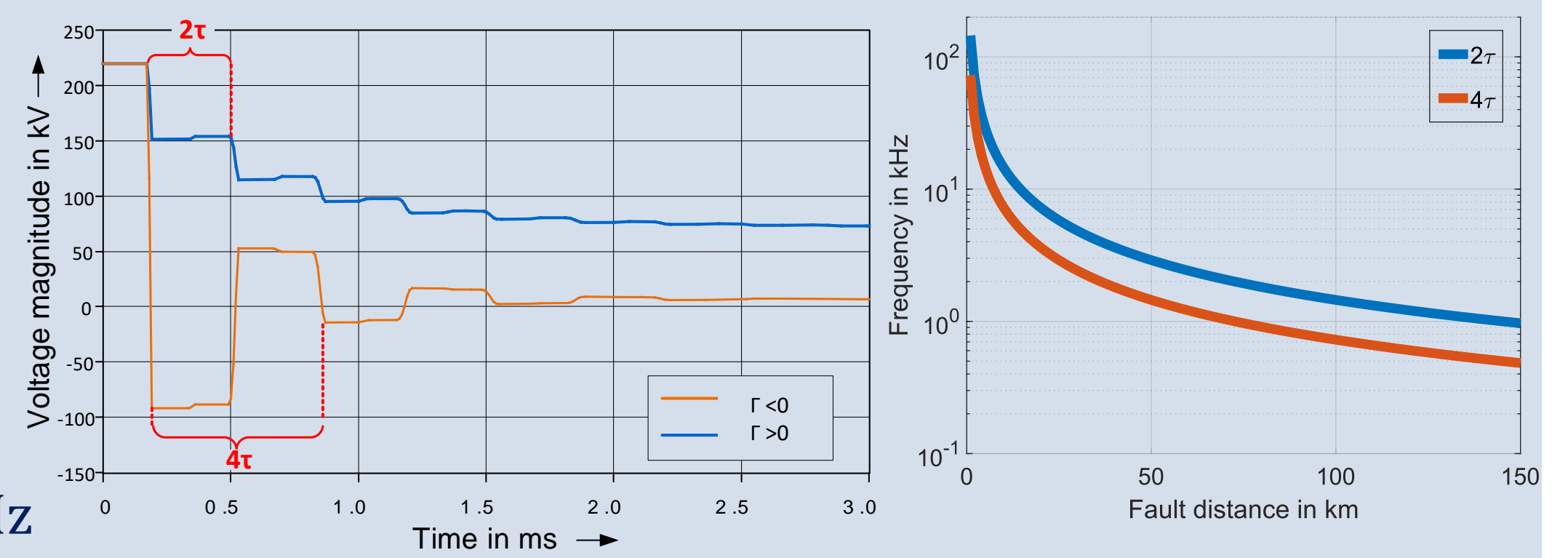
- The control in the phasor quantities, especially in the phase shift of the voltages and currents may cause a confusion in the relay.
- The magnitude of the current negative-sequence of the RES is almost zero, consequently, directional element malfunction may occur.
- The magnitude of the short-circuit current is low (max 1.5 p.u. rated current), this could cause malfunctioning of the overcurrent monitoring algorithms.

Fault-generated High-frequency Transient Signals

Traveling waves (TWs) reflection and refraction.



$$\Gamma_{TW} = \frac{Z_c - Z_0}{Z_c + Z_0} \begin{cases} \Gamma_{TW-} < 0 \rightarrow Freq_{fault} = \frac{1}{4\tau} \text{ Hz} \\ \Gamma_{TW+} > 0 \rightarrow Freq_{fault} = \frac{1}{2\tau} \text{ Hz} \end{cases}$$



$$\tau = \frac{\text{Fault distance}}{\text{TW speed}} = \frac{d}{v}$$

$$v = \frac{1}{\sqrt{LC}} \text{ km/s}$$

$$Z_c = \sqrt{\frac{L}{C}} \Omega$$

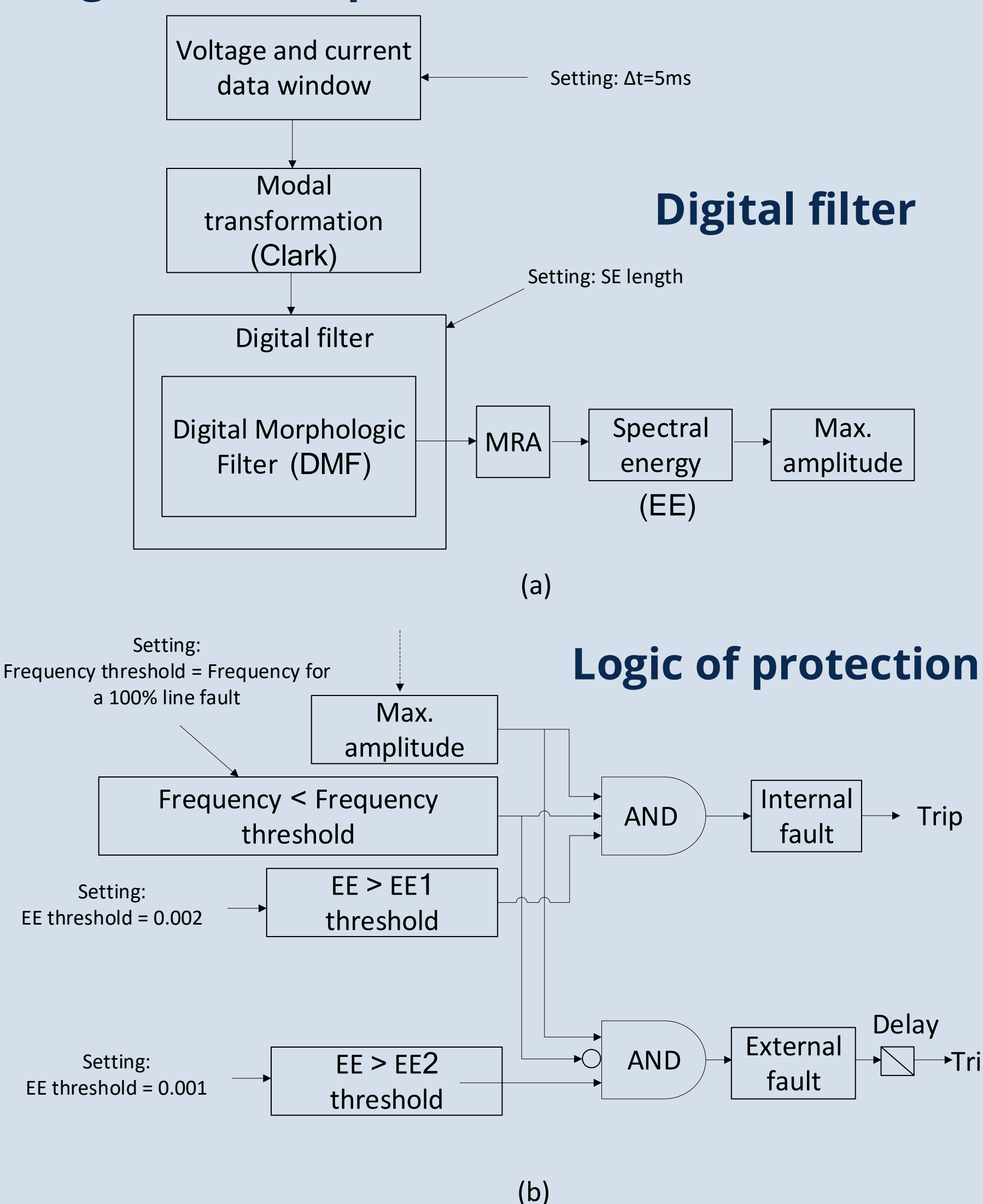
Γ : Reflection coefficient
 Z : characteristic impedance

$Freq_{fault}$: Fault frequency
 τ : Wave travel time from fault to bus L

L : Transmission line impedance
 C : Transmission line capacitance

Methodology and results

Diagram of the protection scheme



Determination of multiresolution signals by means of a morphology filter:

$$DMF_{OC}f(x) = (f \circ g \circ g)(x)$$

$$DMF_{CO}f(x) = (f \circ g \circ g)(x)$$

$$DMF_g f(x) = \frac{DMF_{OC}f(x) + DMF_{CO}f(x)}{2}$$

$$f_n = DMF_{gn} f_{n-1}$$

$$H_n = f_n - f_{n-1}$$

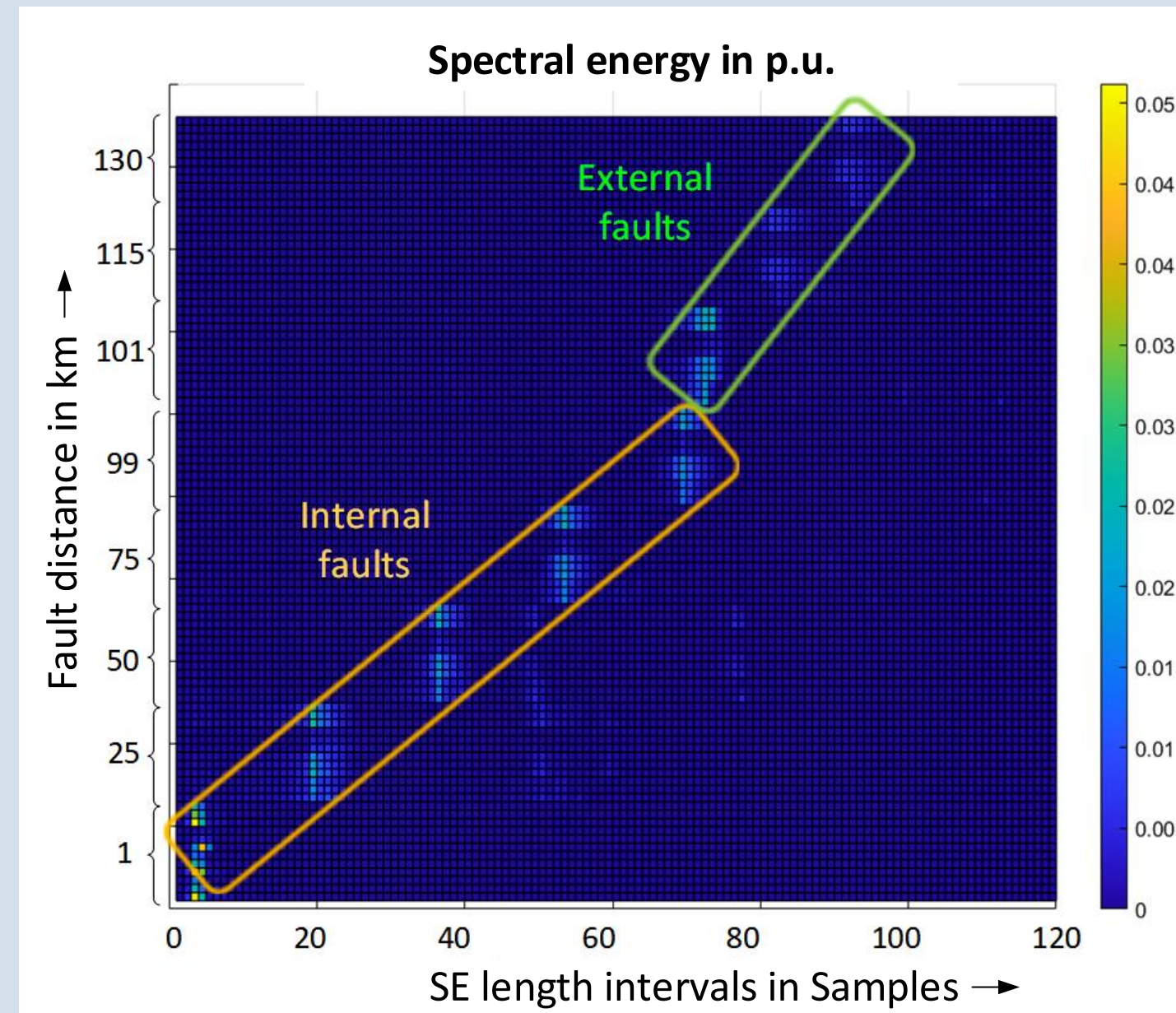
$f(x)$: One-dimensional discrete signal

$g(x)$: Structuring Element (SE)

H_n : Multiresolution signal

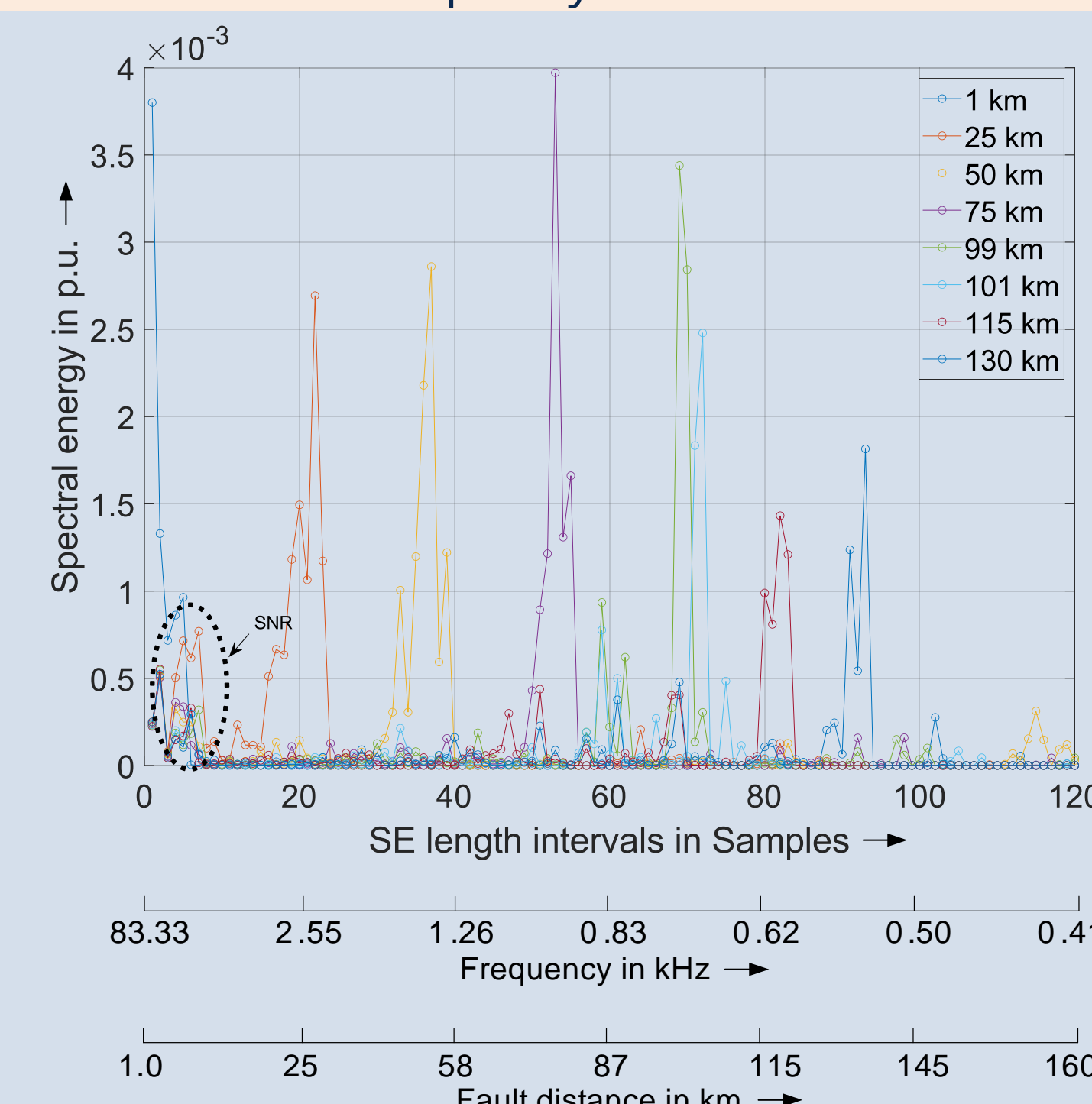
- The SE length defines the frequency of the multiresolution signal.
- The frequency defines the fault location.

Multiresolution spectral energy for different fault location

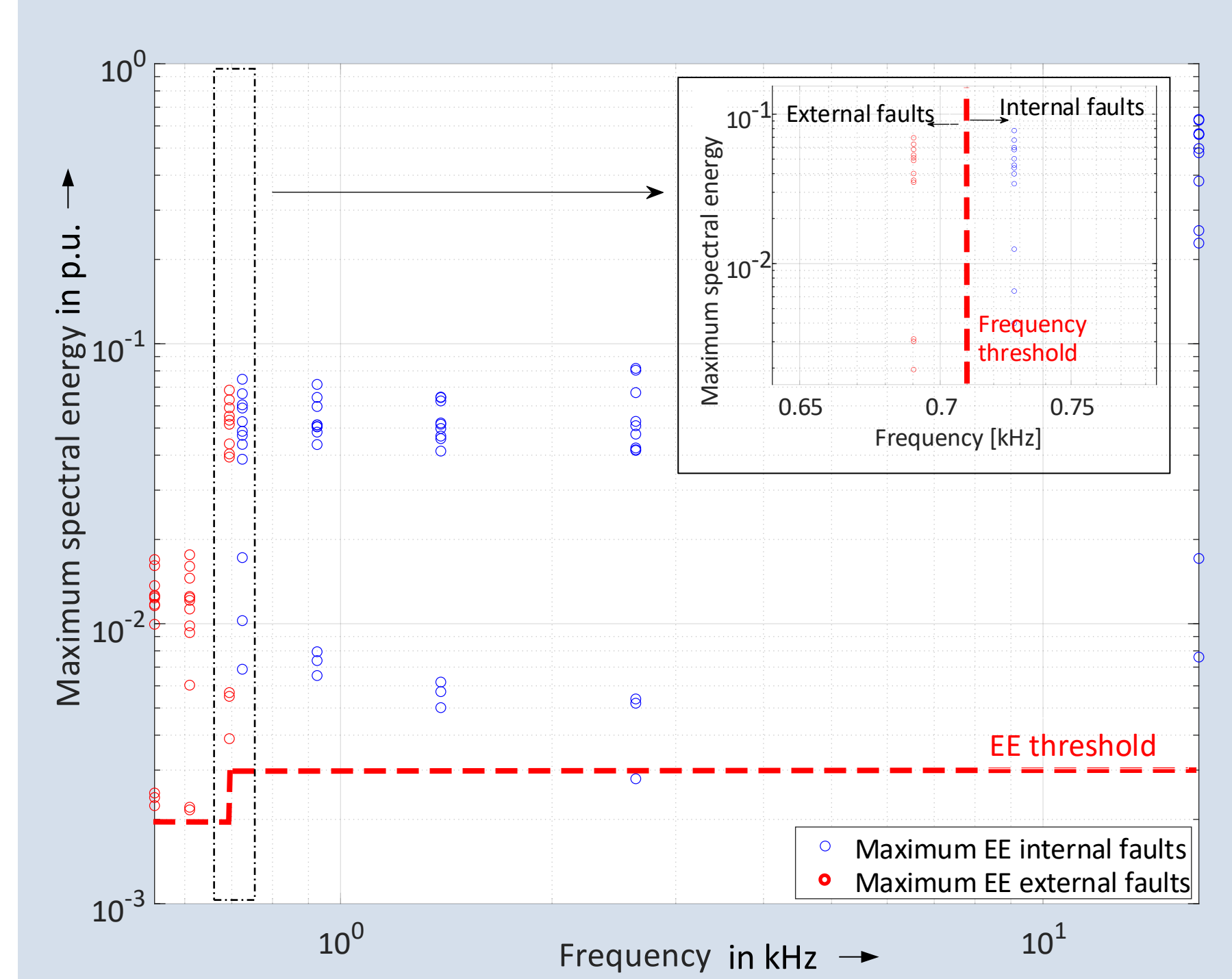


Spectral energy for worst-case scenarios:

- Faults resistance $R=[0-50]$ Ohm
- Insertion angle near zero crossing
- Gaussian noise with signal-to-noise ratio (SNR) of 30 and 40 dB with 10 kHz frequency.



Definition of protection thresholds:



Conclusion

This research proposes a novel distance protection criterion using fault-generated high-frequency transient signals extracted from a digital filter based on mathematical morphology theory. Then, this method can identify internal and external faults of transmission lines.

- Utilize a quarter-cycle time window achieving high-speed, improving system stability and avoiding the effect of inverter's power control system behavior.
- Performs the modal transformation, therefore, it does not need negative-sequence quantities.
- Robust against noise of very-high frequencies (in order of the converter switching frequency) because this method clearly differentiates the noise.
- This method verifies all the factors that influence the fault behavior, such as resistance, insertion angle and location.